

Hot and Cold Utilities in Plant Containing Multiple Heat Exchanger Networks

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Abstract: *In this paper, the hot and cold utilities of a complex natural gas refinery containing multiple heat exchanger networks (HENs) were properly selected. Following using pinch analysis for designing the HENs of the natural gas refinery, this selection could be done by considering available utilities in the plant under consideration. The plant network was divided into the five heat exchanger networks for better and precise estimation of utility requirements in each smaller network. By comparing the type and temperature level of the utility required in each network, the best utility could be selected, in order to use as the heating and cooling media in the plant network with a considerable reduced operating cost of the system. The results show that in the new network design, there was about 38 and 100% reduction in cooling air and BFW respectively, but 45% increase in cooling water, as cold utilities and almost 64.4, 30.0, 90.9 and 100% reduction in HP steam, LP steam, hot flue gas and electric heater as hot utilities, respectively relative to the existing network.*

Keywords: Heat Exchanger Network, Appropriate Placement Principle, Hot and Cold Utilities, Practical Pinch Analysis

1. Introduction

Because of increasing energy costs in recent years, the energy saving methods are usually considered at the early stage of any process design, especially in high energy demand industries such as complex oil and gas refineries. The other important reason for the efficient design of any energy system is mainly due to the environmental regulations, forcing to reduce the amount of pollution gases to the atmosphere [1]. Especially by the more efficient design of the utility system in a huge chemical processing plant, the amount of energy used in the plant life cycle as heating and cooling media will be reduced significantly. In this regard, a variety of optimization methods considering analytical or experimental techniques are available in the literature, showing how it would be possible to design more and more efficient energy systems for various industries [4].

As one of the conceptual methods in process integration, the pinch analysis is widely used as a suitable technique to evaluate and improve the energy systems. The term "Pinch Technology" was introduced by Linnhoff in 1979 to represent a new set of thermodynamically based methods that guarantee minimum energy levels in the design of heat exchanger networks. It is a systematic methodology to achieve utility savings by better process heat integration, maximizing heat recovery and reducing the external utility loads as heating or cooling media in the system. [8] This means in any process integration technique considered for total energy analysis of the systems, the targets for energy saving must be usually set before the design of the heat exchanger network running in the processing plant [9]. In the previous work done by the same authors, it was presented an energy analysis of a complex natural gas refinery by the super-targeting method, showing a considerable saving in yearly energy consumption of the plant [10]. There are a lot of works done in literature and research papers about energy saving techniques using pinch analysis methods, some of them were shown in [10] to [15].

The proper design of the utility system in any processing

industry plays an important role in the operational cost of the system, by increasing or decreasing the heating and cooling requirements of the processing units running in the plant. The most usual types of heating media as hot utilities may include HP or LP steam, hot flue gases from furnaces or fired heaters, hot oil or water, electrical heating and some other less common media. Likewise, cold utilities, which remove heat from the processes by cooling media, may include cooling water or air, chilled water, refrigeration fluids and so on. Usually, the costs of cooling and heating system together with its operational cost are two most important factors for selection of the best utility media in the system. Especially in a huge natural gas refinery as a high energy demand industry, the efficient design of the utility system will considerably affect the energy saving and operational cost of the plant. It is obvious that it provides the key to choosing the correct levels and loads for the various hot and cold utilities. As a case study, the result of pinch analysis in a complex gas refinery which provided by the same authors in [10], was used to analyse the heat exchanger network running in the plant and consider opportunities to select the best heating and cooling media as the utility requirement of the system, using Appropriate Placement principle.

2. Methodology

The method is based on the concept of integration processes and the basic tools which used in the analysis are: Hot and Cold Composite Curves (HCC/CCC), and Grand Composite Curve (GCC). Pinch technology combines heat and mass balance information into simple charts and graphs to show the potential of energy recovery of the heat exchanger network (HEN).

In this analysis, the following steps were considered:

- Extraction of stream data from different processing units, considering the heat and mass balances of all process streams in the network, in order to calculate total heat exchanged required by the cold and hot streams, provided by hot and cold utilities, respectively.
- Drawing the hot and cold composite curves (HCC &

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CCC) as well as grand composite curve (GCC) for all the hot and cold streams in a T-H diagram, to analyze the minimum utility quantities required to solve the heat recovery problem.

- Determine the type and temperature level of utility required as the amount of energy consumption, such as fuel, water, LP and HP steam, refrigerants, air and so on in the network.
- Applying the steps 1 through 3 for all HENs running in the plant under consideration. In the case study of this manuscript, the entire system divided into the five smaller networks (see Table 3 for detail description), each consists of some processing units, so the procedure of utility selection could be applied for all sub-networks in the plant.
- By superposing all the utilities calculated in the previous step for all HENs, the total amount of energy consumption in the utility system of the plant can be determined, and the type and amount of heating and cooling media will be finalized.

3. Choice of Multiple Utility Levels by the Appropriate Placement Principle

The Appropriate Placement principle, originally introduced by Townsend and Linhoff in 1983 [8]. It is obvious that it provides the key to choosing the correct levels and loads for the various hot and cold utilities. Normally, because of cost differentials between utilities, it needs naturally to maximize the use of the least expensive ones. This usually led to maximize the use of the coldest hot utility and the hottest cold utility. The shape of the grand composite often dictates the most appropriate choice of levels and loads. Usually, the trade-offs from using multiple utilities are as follows:

- Steam can often be raised more efficiently at a lower temperature level, as more heat can be recovered from boiler flue gases;
- Power can be generated if the steam is let down from a higher pressure through a turbine;
- Lower-temperature steam is at lower pressure and hence the capital cost of the system is less;
- The driving forces between utilities and process are reduced, so that the surface area and capital cost of heaters/coolers will increase;
- Each extra level increases the complexity of design and incurs an additional capital cost for boilers and pipework.

Hence, according to the above consideration, the designer needs to balance the reduction in running cost against the increased capital cost brought about by increasing the number of levels. Based on the types of utility available in the plant, the external heating and cooling requirements are supplied as a hot and cold utility, at a specified temperatures sufficient to fulfil the duty. Referring to [14], in this case study, the heating media are high and low-pressure steam from steam boilers and hot flue gases from furnaces. The saturated HP steam at 45 bar and 274°C is generated in six gas-fired boilers, followed by let-down stations, in order to produce LP steam at 6.5 bar and 185°C by letting saturated high-pressure steam down to the low-pressure level followed by de-superheating. The hot flue gas delivered by gas-fired heaters, as the heating media with the temperature around

250-400 °C. Cooling media are air, chilled and cooling water and low-temperature propane and ethane as refrigerants. The cooling water is recirculated to a cooling system and returned to the cycle, which works in the range 20–40°C. Air as a cooling medium with the design outdoor temperature of 45°C, is derived by electrical fans in air cooled heat exchangers. The refrigeration system uses propane and ethane between -4.0°C to -90°C.

4. The Case Study: A Brief Description of the Plant

The details of a general gas processing plant were shown in [18]. As the case study of this manuscript, a natural gas refinery designed for refining 2 billion standard cubic feet of natural gas feed per day, delivers 50 million cubic meters per day refined gas injecting to national grid pipeline, 2 million cubic meters per day Ethane, 135 tonnes per day NGL products (propane and butane liquids), 80,000 barrels per day gas condensate and 400 tons per day sulfur solids. The main processing units of the natural gas refinery have been indicated in Table 1. Detail information about this refinery was shown in [10], [11] and [9-12].

Table 1: Main process units of a complex natural gas refinery

UNIT Name	UNIT No.	DESCRIPTION
The gas receiving facilities	Unit 100	Reception Facilities
	Unit 101	Gas Treating
Gas Refining and Liquid Processing	Unit 104	Dehydration and Mercury Guard
	Unit 105	Ethane Recovery
	Unit 106	Export Gas Compression and Metering
	Unit 107	NGL Fractionation
	Unit 109	Sour Water Stripping
	Unit 111	Propane Refrigeration Unit
	Unit 113	Caustic Regeneration Unit for C3 and C4 SULFREX
	Unit 114	Propane Treatment and Drying
	Unit 115	Butane Treatment and Drying
	Unit 116	Ethane Treatment and Drying
	Unit 146	Chemicals Storage
	Unit 147	Propane Storage
	Unit 148	Butane Storage
	Condensate stabilization	Unit 103
Unit 110		Back-up Stabilization
Unit 112		Demercaptinize Condensate (DMC)
Sulfur recovery and storage	Unit 108	Sulfur Recovery
MEG regeneration and re-injection	Unit 102	MEG regeneration
Utility services	Unit 120-132	The utility equipment and accessories (HP/LP Steam, Cooling air and water, Refrigerants and Power generation)

By extraction of all the process and utility data from engineering documents of the plant, the total energy requirements due to the utility consumptions of the plant were determined and summarized in Table 2. According to the Table 2, the cold and hot utilities of the existing plant

were about 213.7 MW and 171.4 MW respectively. Meanwhile, there was 163.5 MW as the available heat recovery in the plant network [10]. According to the results, there was a huge energy consumption to operate the plant, with about 385 MW for the heating and cooling requirements of the process units. Therefore, any improvement in energy saving of the HEN running in the plant, will significantly reduce the annual operational cost, accordingly.

Table 2: Hot and cold utility consumptions in the existing plant

Service	Type of Utility	Consumption (KW)	Total (KW)
Cold Utility	Cooling Air	167,653	213,721
	Cooling Water	46,068	
Hot Utility	HP/LP Steam	160,398	171,422
	Fuel Gas	11,024	
Total Utility Consumption			385,143
Heat Recovery			163,527

5. Results and Discussion

In this plant, the total numbers of hot and cold flow streams were 66 and 44 respectively and the total heat load released by all hot streams is 377,248 KW, whereas total heat load gained by all cold streams is 334,950 KW. The graph of hot and cold composite curves can be developed by drawing all stream temperatures versus cumulative heat loads of hot and cold streams at each temperature level, respectively (Fig. 1).

Referring to the Fig.1, the pinch temperature difference ΔT_{min} in the chart was determined around 66 °C, with the pinch at 97.8 °C shifted temperature, corresponding to 130.8°C for HCC and 64.8 °C for CCC. The Figure shows that total heat recovered by the network is about 163.5 MW, with energy targets of 171.4 MW hot utility and 213.7 MW cold utility.

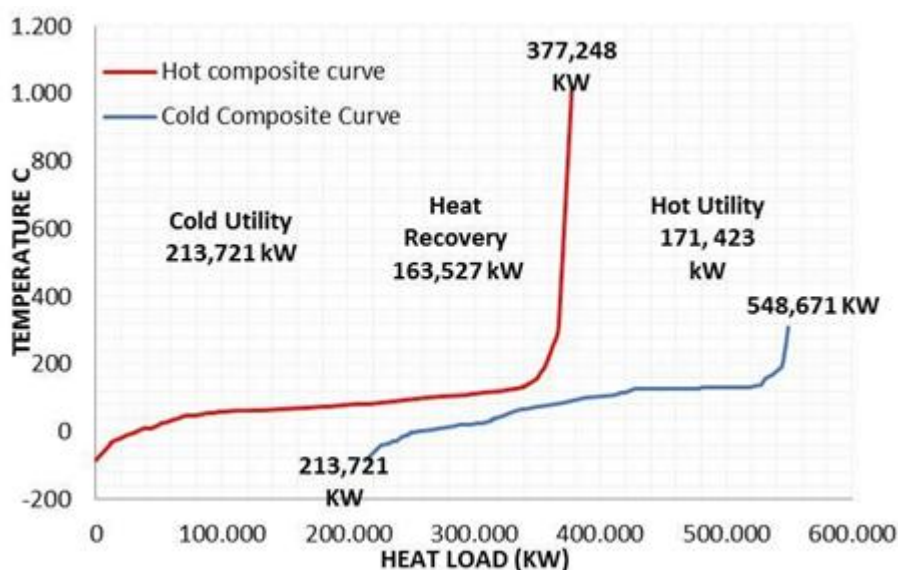


Figure 1: Hot and cold composite curves (HCC/CCC) of the plant network

The plant was divided into the five main areas, each consisting of some neighbor processing units. The nomination of the five areas and the contribution of the process units are shown in Table 3. Therefore, there is a Heat Exchanger Network in each area, consisting of all the heat exchangers located in that area. For more detail information about the plant description and process data, refer to Mehdizadeh Fard et al. [10].

Table 3: Five divided areas in the plant and the relevant assigned units

Zone Number	Unit Number
AREA 1	Units 100/103/109/110
AREA 2	Units 101/104/105/106/111
AREA 3	Units 107/113/114/115/116
AREA 4	Unit 108
AREA 5	Units 146/147/148

The total numbers of heat exchangers in the network are

equal to 104 units with total 208 fluid streams, consisting of 66 hot process streams, 44 cold process streams and 98 utility streams such as HP and LP steams, hot flue gases, cooling water and air. For the details of the hot and cold flow streams, inlet and outlet temperatures, and the heat loads refer to Mehdizadeh Fard et al. [10].

Area No. 1:

By drawing hot and cold composite curves and considering the hot and cold utility requirements from heat balance of the streams in this network, the hot and cold composite curves and grand composite curve were shown in the Figures 2 and 3, respectively. The Figures show that this case was a special type of the pinch analysis, known as threshold problem. In this area, total numbers of hot and cold flow streams were 10 and 13 respectively. The total heat recovered by the network was about 58,707 KW, with energy targets of 33,458 KW hot utility and no cold utility (Fig. 2).

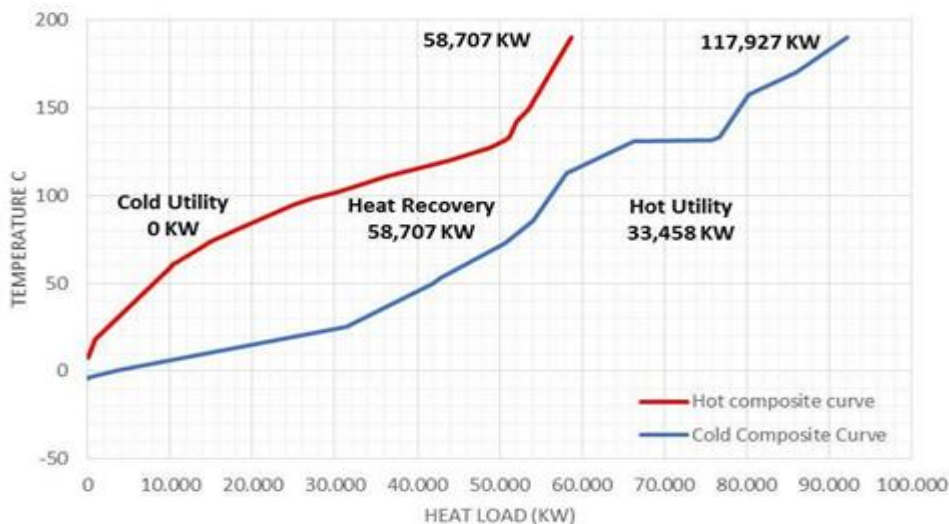


Figure 2: Hot and cold composite curves in Area 1

Referring to the GCC of the network as shown in the Figure 3, the selection of best utility could be done by the Appropriate Placement principle [8]. The type and temperature level of the appropriate utilities were shown in

the Figure 3. It is clear that there are two temperature levels for HP steam as heating media, at 210 C and 160 C, and no cold utility.

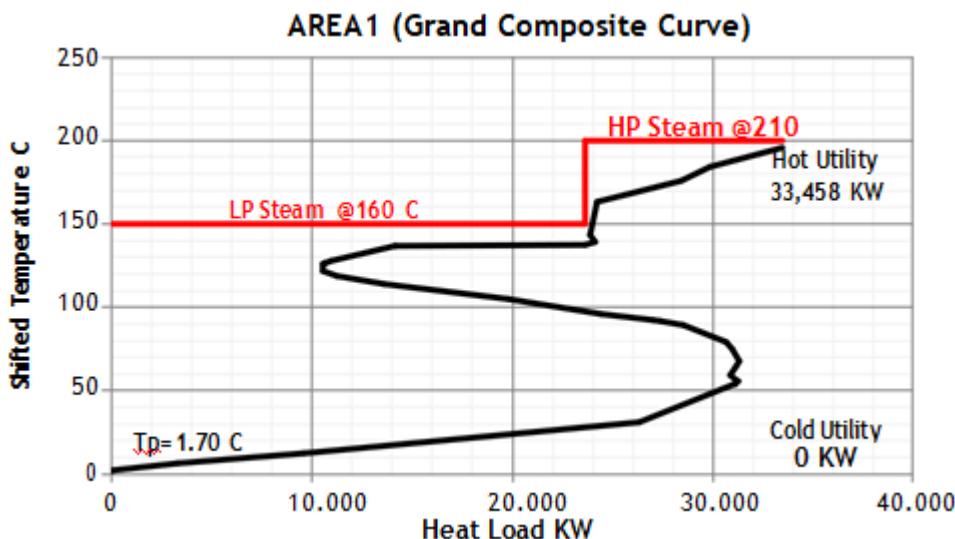


Figure 3: Grand composite curve in Area 1

Area No. 2

By drawing hot and cold composite curves and considering the hot and cold utility requirements from heat balance of the streams in this network, the hot and cold composite curves and grand composite curve were shown in the Figures 4 and 5, respectively. In this area, total numbers of hot and cold flow streams were 13 and 15 respectively. Hot and cold utility requirements of the existing network in this area were about 19,818 KW and 36,300 KW, respectively, with total heat recovered by the network about 99,620 KW (Figure 4)

Referring to the GCC of the network as shown in the Fig. 5, the selection of best utilities could be done by the same procedure explained for Area1 at previous steps. The type and temperature level of the appropriate hot and cold utilities were shown in the same figure. It is clear that there are two temperature levels for the hot utility, i.e. hot flue gas, and HP steam as heating media, and also two temperature levels for the cold utility, i.e. cooling air at 45 C and cooling water at 35 C as cooling media.

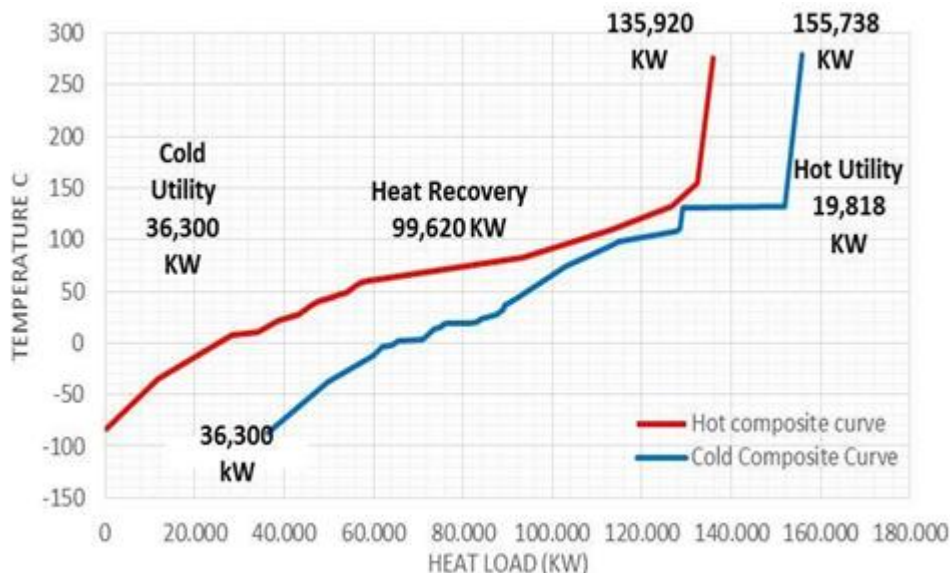


Figure 4: Hot and Cold composite curves in Area 2

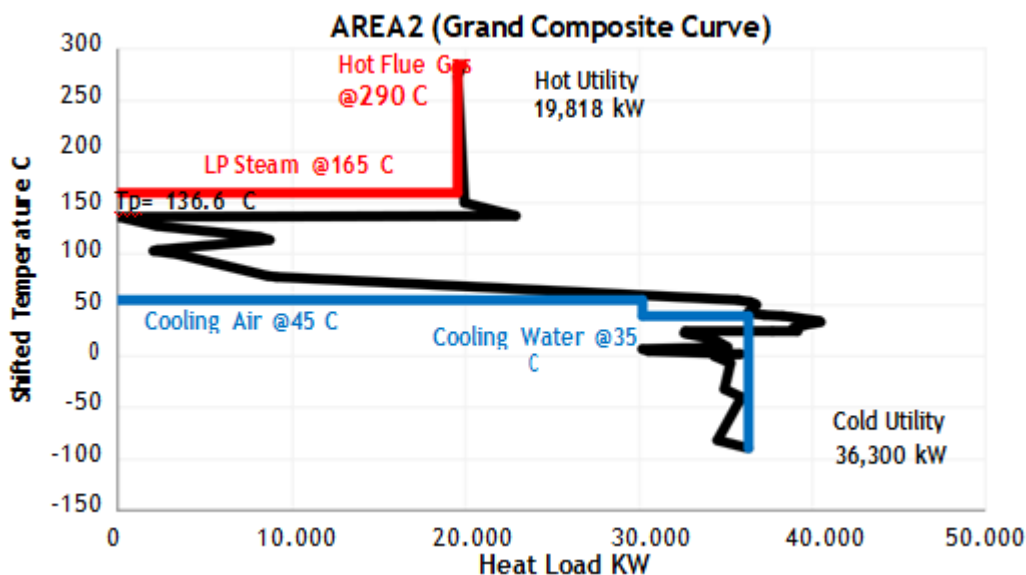


Figure 5: Grand composite curve in Area 2

Area No. 3:

By drawing hot and cold composite curves and considering the hot and cold utility requirements from heat balance of the streams in this network, the hot and cold composite curves and grand composite curve were shown in the Figures 6 and

7, respectively. In this area, total numbers of hot and cold flow streams were 18 and 9 respectively. Hot and cold utility requirements of the existing network in this area were about 26,072 KW and 31,850 KW, respectively, with total heat recovered by the network about 11,837KW (Fig. 6).

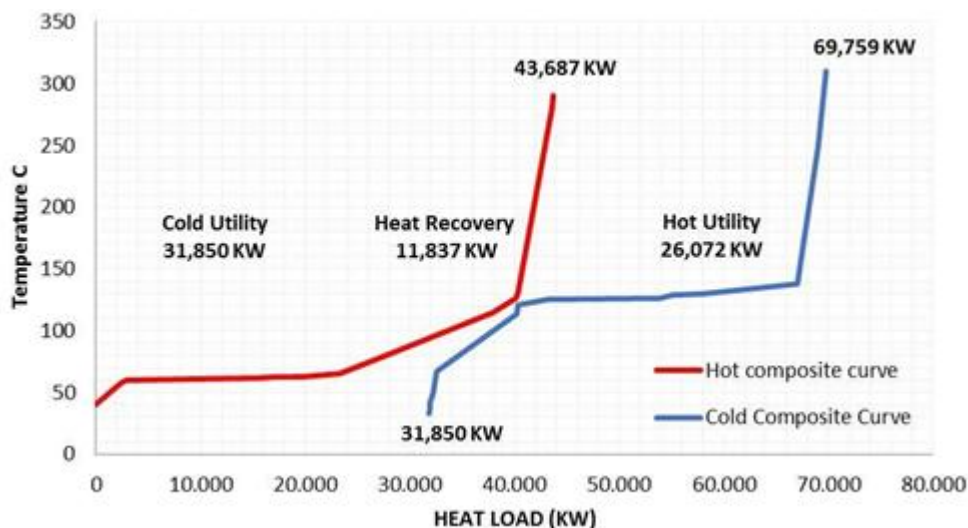


Figure 6: Hot and Cold composite curves in Area 3

Referring to the GCC of the network as shown in the Fig. 7, the selection of best utilities could be done by the same procedure explained for previous networks. The type and temperature level of the appropriate hot and cold utilities were shown in the same figure. It is clear that there are two

temperature levels for the hot utility, i.e. hot flue gas at 320 and HP steam at 160 C as heating media, and two temperature levels for the cold utility, i.e. cooling air at 45 C and cooling water at 30 C as cooling media.

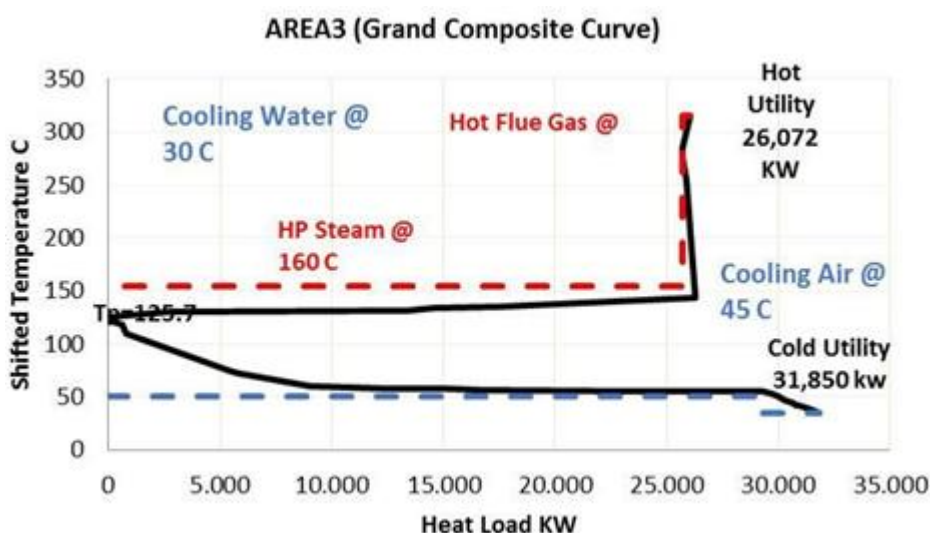


Figure 7: Grand composite curve in Area 3

Area No. 4

By drawing hot and cold composite curves and considering the hot and cold utility requirements from heat balance of the streams in this network, the hot and cold composite curves and grand composite curve were shown in the Figures 8 and 9, respectively. In this area, total numbers of hot and cold flow streams were 12 and 3 respectively. Hot and cold utility requirements of the existing network in this area are about 23,675 KW and 54,348 KW, respectively, with total heat recovered by the network about 49,843 KW (Fig. 8).

Referring to the GCC of the network as shown in the Fig. 9, the selection of best utilities could be done by the same procedure explained in previous steps. The type and temperature level of the appropriate hot and cold utilities were shown in the same figure. It is clear that there is only one temperature level required as the hot utility, i.e. LP steam at 160 C as heating media, but two temperature level as the cold utility, i.e. cooling air and cooling water at 45 C and 30 C respectively, as cooling media.

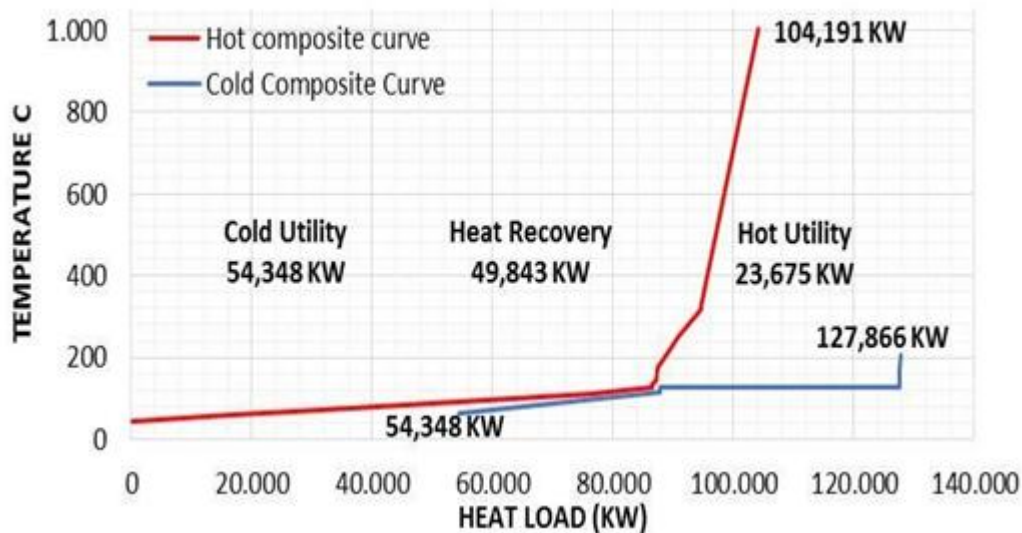


Figure 8: Hot and Cold composite curves in Area 4
AREA4 (Grand Composite Curve)

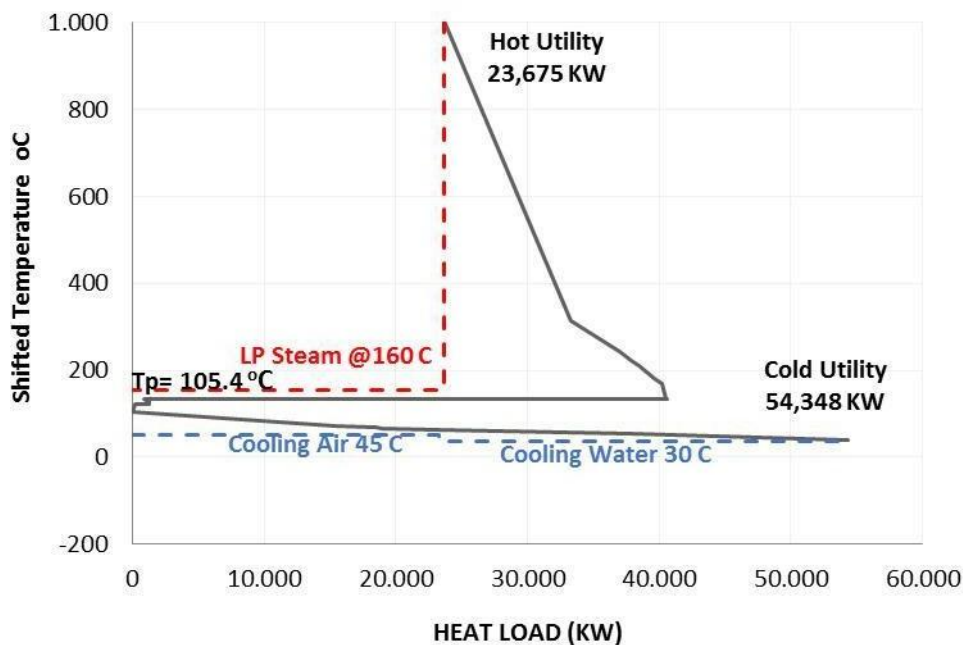


Figure 9: Grand composite curve in Area 4

Area No. 5:

By drawing hot and cold composite curves and considering the hot and cold utility requirements from heat balance of the streams in this network, the hot and cold composite curves and grand composite curve are shown in the Figs. 10 and 11, respectively.

In this area, total numbers of hot and cold flow streams are 10 and 7 respectively. Cold utility requirement of the existing network in this area is about 22,823 KW, and no need to heating media as the hot utility. The graph shows that the heat recovery is equal to 11,920 KW, which is exactly equal to the heat gained by the cold composite curve. Therefore, in this special case, the heat recovery is limited by the total heat received by the cold composite curve (Fig. 10).

Referring to the GCC of the network as shown in the Fig. 11, the selection of best utilities could be done by the same procedure explained in previous steps. The type and temperature level of the appropriate hot and cold utilities

were shown in the same figure. It is clear that there is only one temperature level required as the cold utility, i.e. cooling water at 35 C as cooling media, and no need to the hot utility.

6. Summary of the results from all five HENs

By the combination of the results obtained previously in each area of the refinery, the total energy consumption as the hot and cold utilities could be determined for all networks and the results were shown in Table 4. Meanwhile, the available hot and cold utility of the existing plant networks were summarized in Table 5. The comparison of the results shows that the utility consumption in the new network design would be much better than the existing one, and there is about 35.5% energy saving by applying the pinch analysis of the system. Also, the results show that there is a considerable saving in both heating and cooling media. There is about 32% reduction in cooling air and water, and almost 40%

saving in steam consumption, relative to the existing economic consideration. In addition, the type and temperature level of the heating and cooling media were more reasonable by

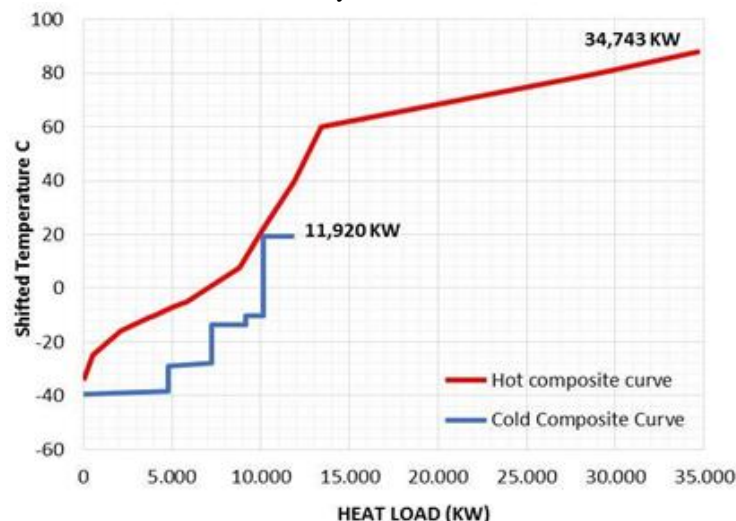


Figure 10: Hot and Cold composite curves in Area 5

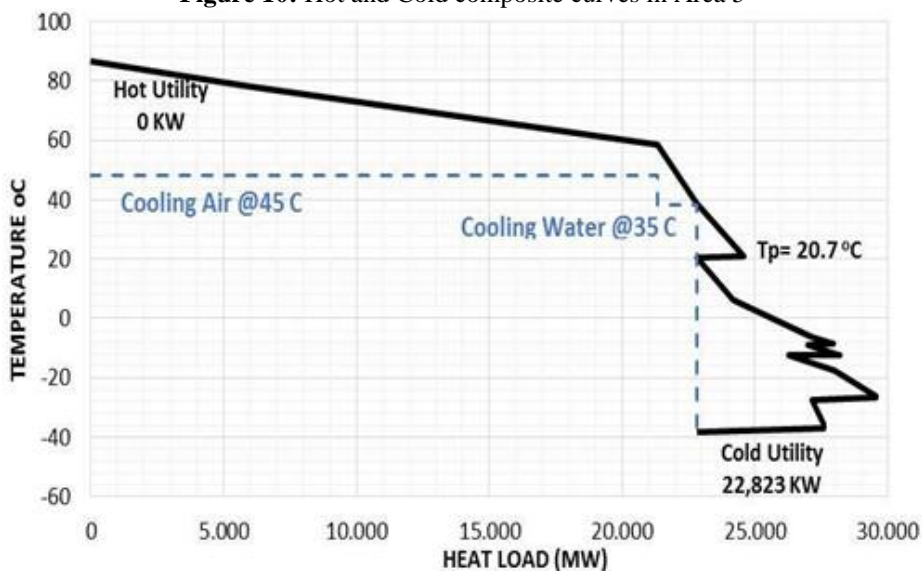


Figure 11: Grand composite curve in Area

The type and temperature level of cooling media were summarized and compared with the existing ones in Table 6. Referring to the table, it was clear that there was about 38 and 100% saving in the total cooling air and BFW consumption respectively, but 45% increase of water consumption as cold utilities.

Meanwhile, the type and temperature level of heating media were summarized and compared with the existing ones in Table 7. Referring to the table, it was clear that there was almost 64.4, 30.0, 90.9 and 100% saving in HP steam, LP steam, hot flue gas and electric heater usage as hot utilities, respectively.

Table 4: Total energy consumption and utility requirement in five networks

TOTAL ENERGY CONSUMPTION IN FIVE HENs (KW)					
Zone No.	Cold Utility		Hot Utility		Total Utility KW
	KW	Type	KW	Type	
Area1	0	-	9,833	HP Steam @210 C	33,458
			23,625	LP Steam @160 C	
Area2	30,190	Cooling Air @45 C	308	Hot Flue Gas @290 C	56,118
	6,110	Cooling Water @35 C	19,510	LP Steam @165 C	
Area3	29,325	Cooling Air @45 C	381	Hot Flue Gas @320 C	57,922
	2,525	Cooling Water @30 C	25,691	LP Steam @160 C	
Area4	23,230	Cooling Air @45 C	23,675	LP Steam @160 C	78,023
	31,118	Cooling Water @30 C			
Area5	21,323	Cooling Air @45 C	0	-	22,823
	1,500	Cooling Water @ 35 C			
All Networks	145,321		103,023		248,344

Table 5: Total energy consumption and utility requirement in five networks (Existing network)

TOTAL ENERGY CONSUMPTION IN FIVE HENs (KW) (Existing Network)					
Zone No.	Cold Utility		Hot Utility		Total Utility KW
	KW	Type	KW	Type	
Area1	23,215	Cooling Air @ 45 C	27,373	HP Steam @ 260 C	79,888
			29,300	LP Steam @ 155 C	
Area2	53,963	Cooling Air @ 45 C	6,426	Hot Flue Gas @ 290 C	1,03,789
			6,173	Cooling Water @ 35 C	
Area3	33,914	Cooling Air @ 45 C	1,125	Hot Flue Gas 350 C	67,954
			2,952	Cooling Water @ 35 C	
Area4	36,738	Cooling Air @ 45 C	246	HP Steam @ 255 C	1,10,689
			16,325	Cooling Water @ 30 C	
			17,618	BFW @ 120 C	
Area5	19,823	Cooling Air @ 45 C	0	-	22,823
All Networks	2,13,721		1,71,422		3,85,143

Table 6: Total cold utility requirement in five networks

Comparison of total cold utilities in exiting network & network after utilities selection following pinch analysis			
Zone No.	Exiting network	Network after the utilities selection following pinch analysis	Percent Change in Cold Utility
Area1	23,215 KW Cooling Air @ 45 C	0	100%
	53,963 KW Cooling Air @ 45 C	30,190 KW Cooling Air @ 45 C	44.10%
Area2	6,173 KW Cooling Water @ 35 C	6,110 KW Cooling Water @ 35 C	1.00%
	33,914 KW Cooling Air @ 45 C	29,325 KW Cooling Air @ 45 C	13.50%
Area3	2,952 KW Cooling Water @ 35 C	2,525 KW Cooling Water @ 30 C	14.50%
	36,738 KW Cooling Air @ 45 C	23,230 KW Cooling Air @ 45 C	36.80%
	16,325 KW Cooling Water @ 30 C	31,118 KW Cooling Water @ 30 C	-90.60%
Area4	17,618 KW BFW @ 120 C	0	100%
	19,823 KW Cooling Air @ 45 C	21,323 KW Cooling Air @45 C	-7.60%
Area5	3,000 KW Cooling Water @ 30 C	1,500 KW Cooling Water @ 35 C	50%
All Networks (KW)	167,653 KW; Cooling Air @ 45 C	104,068 KW; Cooling Air @ 45 C	37.90%
	28,450 KW; Cooling Water @ 30 & 35 C	41,253 KW; Cooling Water @ 30 & 35 C	-45.00%
	17,618 KW; BFW @ 120 C	0 KW; BFW @ 120 C	100%

Table 7: Total hot utility requirement in five networks

Comparison Of hot utilities in exiting network & network after utilities selection following pinch analysis			
Zone No.	Exiting network	Network after the utilities selection following pinch analysis	Percent Reduction in Hot Utility
Area1	27,373 KW HP Steam @ 260 C	9,833 KW HP Steam @ 210 C	64.1%
	29,300 KW LP Steam @ 155 C	23,625 KW LP Steam @ 160 C	19.4%
Area2	6,426 KW Hot Flue Gas @ 290 C	308 KW Hot Flue Gas @ 290 C	95.2%
	37,227 KW LP Steam @ 155 C	19,510 KW LP Steam @ 165 C	47.6%
Area3	1,125 KW Hot Flue Gas @ 350 C	381 KW Hot Flue Gas @ 320 C	95.2%
	3,473 KW Electric Heater	0	100%
	26,490 KW LP Steam @ 155 C	25,691 KW LP Steam @ 160 C	3.0%
Area4	246 KW HP Steam @ 255 C	0	100%
	39,762 KW LP Steam @ 145 C	23,675 KW LP Steam @ 160 C	40.5%
Area5	0	0	-
All Networks (KW)	27,619 KW HP Steam @ 255 & 260 C	9,833 KW HP Steam @ 210 C	64.4%
	132,779 KW LP Steam @ 145 & 155 C	92,501 KW LP Steam @ 160 & 165 C	30%
	7,551 KW Hot Flue Gas @ 290 & 350 C	689 KW Hot Flue Gas @ 290 & 320C	90.9%
	3,473 KW Electric Heater	0	100%

7. Conclusion

As one of the conceptual methods in process integration, the pinch analysis is widely used as a suitable technique to evaluate and improve the energy systems. As a case study, the natural gas refinery of the South Pars Gas field in the Persian Gulf was chosen analyzed for energy requirement, in order to identify the type and temperature of appropriate utility as heating and cooling media in the total system.

The new network design improves total energy consumption about 35.52% relative to the existing one. Hot and cold utilities in the new network were 103,023 and 145,321 KW, respectively while the hot and cold utilities in the exiting network were 171,422 and 213,721 KW, respectively. Also, the results show that there was a considerable saving in both heating and cooling media. In this case study, there was about 38 and 100% reduction in cooling air and BFW respectively, but 45% increase in cooling water, as cold utilities, and almost 64.4, 30.0, 90.9 and 100% reduction in

HP steam, LP steam, hot flue gas and electric heater as hot utilities, respectively relative to the existing network.

In many cases, this method can be targeted for both energy and cost savings achieved at the same time, by selection of the best utilities as heating and cooling media. The result shows that in addition to the energy saving in the new network design, the distribution of utility media in heating and cooling processes were much better than the existing network.

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