A New Cascade H-Bridge Inverter Based Multi-Level Statcom for High Power Applications

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Abstract: The industrial power sector and domestic power sector requires bulk power transfer from sources, in which reactive power and power quality (PQ) are the major issues. This paper presents a cascaded H-bridge inverter based multi-level static compensator (STATCOM) using space vector pulse width modulation technique (SVPWM). The main objective is reactive power compensation with improved power quality. The topology consisting of two standard H-bridge inverters connected through a three-phase transformer. In high power applications, VAR compensation is achieved using multi-level inverters. The SVPWM is the best reliable advanced modulation technique, enables better DC bus utilization. In addition, SVPWM produces fewer harmonics in the output voltage and current thus gives quality of power. The performance of the scheme is analysed through MATLAB/SIMULINK.

Keywords: Power Quality (PQ), Static Compensator (STATCOM), Space Vector Pulse Width Modulation (SVPWM), Volt-Ampere Reactive (VAR).

1. Introduction

Generation and transmission of power is a complex process, it requires working of many components to produce maximum output. In which, the main component is reactive power in the system. To deliver the required active power through transmission lines, voltage is needed to be maintained. Reactive power is required for operation of loads such as motor loads and other inductive loads [1]. The performance of ac power system can be improved by maintaining this reactive power efficiently and which is generally called as reactive power compensation [2]-[3]. The reactive power compensation is associated with load compensation and voltage support [8]-[9]. In recent years, static VAR compensators like the STATCOM have been developed [4]-[5]. These static VAR compensators come under Flexible AC Transmission Systems (FACTS) and it can absorb or generate the reactive power if it is required.

It is difficult to operate medium voltage grids with a single power semiconductor switch directly. Therefore multi-level inverters have been preferred for higher voltage levels. In industrial applications, multi-level inverters have more attention. These inverters can be used as static VAR compensators and also used in renewable energy systems, motor drives etc. [7]-[8]. Generally multilevel inverters have output voltage levels of more than two levels. This leads to generate reduced harmonic distortions in the output voltages and high quality output waveforms. Additionally, these inverters can have fraction of dc-link voltages when batteries, capacitors are used as sources. Multi-level inverters with these characteristics can be best suited for high-power and high-voltage applications. In multi-level family cascade Multilevel Inverter (CMI) is one of the best topology due to its own advantages than other inverters [2]. The control of dc-link voltage of inverter is illustrated [10]-[11].

These inverters have been implemented with various PWM techniques [13] to control the output voltage and frequency also for better DC-AC power conversion. In the other hand, the usage of space vector pulse width modulation technique has been increased in last decade due to several advantages such as reduced total harmonic distortion (THD) and commutation losses. Thus quality power is achieved with these techniques.

The Overall paper is organized as follows: The section I presents introduction about the proposed system. Section II represents control scheme and proposed system description. Section III represents the concept of space vector pulse width modulation technique. Section IV represents Simulink model results respectively. Overall conclusion is shown in section V.

2. System Modelling and Description

The power system and STATCOM model is shown in Fig.1. This model represents the connection point of STATCOM in the power system.

Figure 1: Power system and the STATCOM model

The schematic diagram of cascaded two-level inverter based multi-level STATCOM is shown in Fig.2. In which the low-voltage (LV) side and high voltage (HV) side of a transformer is connected to inverter and grid respectively.
A. Phase Equivalent Circuit

Equivalent circuit of phase „a” is shown in Fig.4. In the figure, the RMS source voltage is represented as \( v_a \). The transformer winding inductance is represented as \( L \), the voltage across primary side of the transformer of inverter1 and inverter2 is \( (e_{a1}-e_{a2}) \).

Applying KVL to the loop

\[-v_a + R_a i_a' + L_a \frac{di_a'}{dt} + (e_{a1}-e_{a2}) = 0 \]

Similarly for „b” and „c” phases

\[-v_b + R_b i_b' + L_b \frac{di_b'}{dt} + (e_{b1}-e_{b2}) = 0 \]

\[-v_c + R_c i_c' + L_c \frac{di_c'}{dt} + (e_{c1}-e_{c2}) = 0 \]

By assuming resistances \( R_a = R_b = R_c = R \) and inductances \( L_a = L_b = L_c = L \), the above can be written in mathematical model form as,

\[ \begin{bmatrix} \frac{di_a'}{dt} \\ \frac{di_b'}{dt} \\ \frac{di_c'}{dt} \end{bmatrix} = \begin{bmatrix} -\frac{1}{L} & 0 & 0 \\ 0 & -\frac{1}{L} & 0 \\ 0 & 0 & -\frac{1}{L} \end{bmatrix} \begin{bmatrix} i_a' \\ i_b' \\ i_c' \end{bmatrix} + \frac{1}{L} \begin{bmatrix} v_a - (e_{a1} - e_{a2}) \\ v_b - (e_{b1} - e_{b2}) \\ v_c - (e_{c1} - e_{c2}) \end{bmatrix} \]

The equation (4) is known as mathematical model in the stationary reference form of cascaded two-level inverter based STATCOM. To control both the active and reactive currents independently, above stationary reference frame equations can be converted into rotating reference frame equations. The source voltage of q-component is set to be zero so that the source voltage of d-component can be aligned with the synchronously rotating reference frame.

The dynamic model in the synchronously rotating reference frame is given as

\[ \begin{bmatrix} \frac{de_d}{dt} \\ \frac{de_q}{dt} \end{bmatrix} = \begin{bmatrix} -\frac{\omega}{L} & \frac{1}{L} \\ \frac{\omega}{L} & -\frac{1}{L} \end{bmatrix} \begin{bmatrix} i_d' \\ i_q' \end{bmatrix} + \frac{1}{L} \begin{bmatrix} v_d - (e_{d1} - e_{d2}) \\ -v_q - (e_{q1} - e_{q2}) \end{bmatrix} \]

Here \( v_d' \) represents the direct (d)-axis voltage component of ac source and \( i_d' \), \( i_q' \) represents d-axis and q-axis current components of cascaded two-level inverter.

B. Control Strategy

The block diagram of control circuit is shown in Fig. 5. The d-axis and q-axis voltages can be controlled as follows

\[ e_d^* = -x_1 + \omega_L i_q' + v_d' \]

\[ e_q^* = -x_2 - \omega_L i_q' + v_q' \]

Where \( e_d^* \) and \( e_q^* \) represents d-axis and q-axis reference voltage components of the inverter. The parameters \( x_1 \) and \( x_2 \) are known as control parameters and these can controlled as

\[ x_1 = (k_{p1} + \frac{k_{d1}}{s})(i_d' - i_d^*) \]

\[ x_2 = (k_{p2} + \frac{k_{d2}}{s})(i_q' - i_q^*) \]

Where \( i_d^* \) is the direct (d)-axis reference current and is given by

\[ i_d^* = (k_{p3} + \frac{k_{d3}}{s})(V_{dc1} + V_{dc2}) \]

Where \( V_{dc1} \) and \( V_{dc2} \) represents the reference voltages of dc-link capacitors of inverter 1 and inverter 2. The reference reactive current component i.e q-axis component \( i_q^* \) is obtained either from load, when used for load compensation or from voltage regulation loop when used in transmission lines.

Fig.5 Shows that the three phase voltages \( v_a, v_b, v_c \) are given to phase-locked loop (PLL) to generate the unit signal \( \cos \omega t \) and \( \sin \omega t \). Phase lock loop or phase locked loop (PLL) is a type of control system, which is used to generate output signal to match the phase of input signal. These unit signals are used to transform the converter currents \( i_a, i_b, i_c \) into synchronously rotating reference frame currents. So that it is easy to control reactive and active current components. These currents consist of large switching frequency ripples and which are eliminated by using low-pass filters (LPF). The reference voltages to the converter are \( e_d^*, e_q^* \) are generated from controller using \( (V_{dc1} + V_{dc2}) \) and \( i_q^* \). The inverter supplies desired reactive
component of current $i_{q1}^*$ and draws active component of current $i_{d1}^*$ by considering these reference current components. Which can be further used to regulate total dc-link voltage $V_{dc1}^* + V_{dc2}^*$ of the inverter.

The control circuit uses the sinusoidal pulse width modulation (SPWM) technique to generate gate signals from the obtained reference voltages.

The relation between line-line output voltage in vector form \( [V_a V_b V_c] \) and switching variables vector \([abc]\) is given by the equation
\[
\begin{align}
V_{abc} &= [1 -1 0] \begin{bmatrix} V_a \\ V_b \\ V_c \end{bmatrix} \\
V_{abc} &= [0 1 -1] \begin{bmatrix} V_a \\ V_b \\ V_c \end{bmatrix} \\
V_{abc} &= [-1 0 1] \begin{bmatrix} V_a \\ V_b \\ V_c \end{bmatrix}
\end{align}
\] (15)

Similarly for phase voltage vector relation is given by
\[
\begin{align}
V_a &= \frac{1}{3} V_{dc} [2 -1 -1] \\
V_b &= \frac{1}{3} V_{dc} [-1 2 -1] \\
V_c &= \frac{1}{3} V_{dc} [-1 -1 2]
\end{align}
\] (16)

Where $V_{dc}$ is dc bus voltage or supply voltage. The maximum line to line and phase output voltage achieved by SVPWM is given by
\[
V_{phmax} = \frac{V_{dc}}{2} \quad \text{and} \quad V_{limax} = V_{dc}
\] (17)

The three phase voltages of a three phase inverter are $V_a$, $V_b$ and $V_c$ respectively. The six power transistor switches $Q_1$ to $Q_6$ are controlled by switching variables $a$, $a' b$, $b'$ and $c$, $c'$. The working principle is when upper switches are turned ON i.e $a$, $b$ or $c$ is $1$, corresponding lower switches are turned OFF i.e $a$, $b$ or $c$ is $0$. The ON and OFF of upper switches $Q_1$, $Q_2$ and $Q_3$ are used to determine the output voltage.

The upper power transistor switches ON and OFF states gives eight possible combinations i.e six non zero vectors and two zero vectors. The six non zero vectors are $(V_{a1} V_{b1} V_{c1})$ gives hexagonal shape and zero vectors are $(V_{a2} V_{b2} V_{c2})$.

The eight combinations and phase or line voltages in terms of supply voltage $V_{dc}$ is given in table.

<table>
<thead>
<tr>
<th>Voltage vectors</th>
<th>Switching vectors</th>
<th>Phase voltage</th>
<th>Line to Line voltage</th>
</tr>
</thead>
<tbody>
<tr>
<td>$V_a$</td>
<td>0 0 0</td>
<td>0 0 0</td>
<td>0 0 0</td>
</tr>
<tr>
<td>$V_b$</td>
<td>0 0 0</td>
<td>2/3 -1/3 -1/3</td>
<td>1 0 -1</td>
</tr>
<tr>
<td>$V_c$</td>
<td>0 0 0</td>
<td>1/3 -1/3 -1/3</td>
<td>1 0 -1</td>
</tr>
<tr>
<td>$V_d$</td>
<td>0 0 0</td>
<td>2/3 -1/3 -1/3</td>
<td>1 0 -1</td>
</tr>
<tr>
<td>$V_e$</td>
<td>0 0 0</td>
<td>1/3 -1/3 -1/3</td>
<td>1 0 -1</td>
</tr>
<tr>
<td>$V_f$</td>
<td>0 0 0</td>
<td>1/3 -1/3 -1/3</td>
<td>1 0 -1</td>
</tr>
<tr>
<td>$V_g$</td>
<td>0 0 0</td>
<td>1/3 -1/3 -1/3</td>
<td>1 0 -1</td>
</tr>
<tr>
<td>$V_h$</td>
<td>0 0 0</td>
<td>1/3 -1/3 -1/3</td>
<td>1 0 -1</td>
</tr>
</tbody>
</table>

By assuming d-axis is fixed horizontal axis and q-axis fixed vertical axis, the phase voltage representation in the vector form with the eight switching patterns can be obtained by the d-q transformation to the phase voltages.

\[
T_{abc-dq} = \frac{\sqrt{3}}{2} \begin{bmatrix} 1 & -1/2 & -1/2 \\
0 & \frac{\sqrt{3}}{2} & -\frac{\sqrt{3}}{2} \\
0 & 0 & \frac{\sqrt{3}}{2} \end{bmatrix}
\] (18)
This d-q transformation is equivalent to orthogonal trajectory of \([a, b, c]^{T}\) on to two dimensional perpendicular to vector \([1,1,1]^{T}\) in the three-dimensional co-ordinate system. This results six non-zero and two zero vectors are possible. The six non-zero vectors \((V_1, V_2, V_3, V_4, V_5, V_6)\) shapes the axis of hexagonal, supplies power to the load connected shown in figure. The zero vectors \((V_0, V_7)\) are at the origin and supplies zero voltage to the load.

The main objective of SVPWM technique is approximate the reference voltage \(V_{out}\) instantaneously by using eight switching combination corresponding to the basic space vectors. One of the simple way of approximation is generate switching combination corresponding to the basic space reference voltage \(V_{out}\) with in small time of \(T\), then equation (19) becomes (20), Where \(T_1 + T_2 < T\). The time \(T\) small with the change in speed of \(V_{out}\), so it becomes critical. In practical, approximation is for every time period \(T_{pwm}\).Therefore it is too difficult that to have small time period \(T\) with respect to change in \(V_{out}\).

\[
V_{out} (nT) = \frac{1}{T} \left( T_1 V_x + T_2 V_{x \pm 60} \right) \\
V_{out} (nT + T) = \frac{1}{T} \left( T_1 V_x + T_2 V_{x \pm 60} \right) 
\]

In the equation \(T_1, T_2\) are time duration to the switching states corresponding to \(V_x\) and \(V_{x \pm 60}\) (or \(V_{x \pm 60}\)) are applied. The \(V_x\) and \(V_{x \pm 60}\) (or \(V_{x \pm 60}\)) are basic space vectors formed by the sector containing of \(V_{out}\). If we assume change in reference voltage \(V_{out}\) with in small time of \(T\), then equation (19) becomes (20). Where \(T_1 + T_2 < T\). The time \(T\) is small with the change in speed of \(V_{out}\), so it becomes critical. In practical, approximation is for every time period \(T_{pwm}\).Therefore it is too difficult that to have small time period \(T\) with respect to change in \(V_{out}\).

Equation (20) is for every PWM period, approximate the \(V_{out}\) with the inverter is in switching states \(V_x\) and \(V_{x \pm 60}\) (or \(V_{x \pm 60}\)) for time duration of \(T_1\) and \(T_2\) respectively. The sum of time durations \(T_1\) and \(T_2\) should be less than or equals to \(T_{pwm}\) and inverter should be at the origin in rest of the period. Therefore equation (20) becomes (22), where

\[
T_{pwm} V_{out} = T_1 V_x + T_2 V_{x \pm 60} + T_0 \left( V_0 \text{ or } V_7 \right) 
\]

We get the \(T_1, T_2\) equation from the (22) equation

\[
\begin{align*}
(T_1; T_2) &= T_{pwm} [V_x; V_{x \pm 60}]^{-1} V_{out} 
\end{align*}
\]

Here \([V_x; V_{x \pm 60}]^{-1}\) is known as normalized decomposition matrix for the sectors. If we assume the angle between \(V_x\) and \(V_{out}\) is then for time durations \(T_1\) and \(T_2\) is

\[
T_1 = \sqrt{2} T_{pwm} ||V_{out}|| \cos (\alpha + 30^0) \\
T_2 = \sqrt{2} T_{pwm} ||V_{out}|| \sin (\alpha)
\]

Advantages of SVPWM are

- SVPWM utilizes the dc bus voltage efficiently and generates the less total harmonic distortions (THD) compared to the SPWM.
- Low switching losses and wide modulation range is possible.
- Higher fundamental voltage magnitude i.e \(15.5\%\) more over SPWM.
- Variable fundamental voltage magnitude control and lower power losses.

Table 2: Shows the different system parameters used in simulation

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Rated power</td>
<td>5 MVA</td>
</tr>
<tr>
<td>Transformer voltage rating</td>
<td>11KV/400</td>
</tr>
<tr>
<td>AC supply frequency, f</td>
<td>50 Hz</td>
</tr>
<tr>
<td>Inverter-1 dc link voltage, Vdc1</td>
<td>659 V</td>
</tr>
<tr>
<td>Inverter-2 dc link voltage, Vdc2</td>
<td>241 V</td>
</tr>
<tr>
<td>Transformer leakage reactance, (X_t)</td>
<td>15%</td>
</tr>
<tr>
<td>Transformer resistance, (R)</td>
<td>3%</td>
</tr>
<tr>
<td>DC link capacitances, (C_1, C_2)</td>
<td>50 mF</td>
</tr>
<tr>
<td>Switching frequency</td>
<td>1200 Hz</td>
</tr>
</tbody>
</table>

### 4. Simulation Results

#### A. Reactive power control

Fig.8 shows the waveforms of source voltage inverter current, DC-link voltage of two inverters in the reactive power control case.
In this case reactive power is controlled by setting $i_q^*$ i.e. reference reactive current component at a particular reference value. Initially $i_q^*$ is set at 0.5 p.u. At $t=2.0$ s, $i_q^*$ is changed from 0.5 to -0.5. DC-link voltage of two inverters are regulated during the STATCOM modes are changed.

**B. Load compensation**

In this case, reactive power of the load is compensated by the STATCOM. Initially STATCOM supplies the current of +0.5 p.u. When load current increases at $t=2.0$ s, STATCOM supplies more than +0.5 p.u. Therefore load compensation is effectively achieved by the STATCOM. The DC-link voltages of two inverters $V_{dc1}$ and $V_{dc2}$ are regulated at their respective values when STATCOM operating modes are changed.

**C. Operating during the fault condition**

Fig.10 shows the waveforms of grid voltages on LV side of the transformer, during the fault condition. In which, a single line to ground fault is created at 1.2s and cleared after 200 ms on A phase of HV side of the 33/11 kv transformer. The corresponding d-q axis currents of the inverter are shown. The fault currents are regulated at their respective values i.e at zero.

**5. FFT Analysis**

The frequency spectrum of different signals is obtained by this FFT analysis.

**Figure 8:** a) Source voltage and Inverter current b) DC-link voltages of two inverters

**Figure 9:** a) Source voltage and inverter current b) DC-link voltages of two inverters

**Figure 10:** a) Grid voltages on the LV side of the transformer b) d-axis negative sequence current component c) q-axis negative sequence current component

**Figure 11:** FFT Analysis showing THD of load voltage by using SPWM&SVPWM

Powergui block can be used to obtain the frequency spectrum of any signal directly. The bar graph shows the order of
harmonics and its magnitude. FFT analysis is carried out to study the harmonic spectrum of load voltage and load current before and after using SVPWM. By using SVPWM the THD load voltage reduced from 8.32% to 1.69%. The THD of load voltage with SPWM and SVPWM is shown in table.

<table>
<thead>
<tr>
<th>Inverter modulation technique</th>
<th>THD in Load voltage (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Sinusoidal Pulse width modulation</td>
<td>8.32</td>
</tr>
<tr>
<td>Space Vector Pulse width modulation</td>
<td>1.69</td>
</tr>
</tbody>
</table>

6. Conclusion

This paper presents cascaded H-bridge inverter based multi-level static compensator (STATCOM) using space vector pulse width modulation technique (SVPWM). The main objective is to compensate the reactive power with the improved power quality. Sinusoidal pulse width modulation have better control on output voltage magnitude, they accounts for harmonics in the output voltage. By using space vector pulse width modulation the total harmonic distortion can be further reduced and it has various advantages than the SPWM. The scheme is analysed at various operating conditions. SVPWM reduces the THD of load voltage from 8.32% to 1.69%. Thus power quality is improved with reactive power compensation.

References


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