# Power Estimation of HCFV Based on Voyage Profile

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Abstract: The hybrid technology, when applicable for sea transportation, is a way to reduce the use of fossil fuels and toxic gases. The hybrid power of catamaran fishing vessel (HCFV) is designed to use a combination power by using engine electric and sail. The configuration consist of individual power and combined power (diesel engine and sail, diesel engine and solar panels, and sail, solar panels and diesel engine). The method of power estimation using the experiment result of catamaran resistance in towing tank [1], and followed by calculating the thrust requirement (T req.) and estimating the energy of power (P req.) of individual and later the combined power based on fishing vessel transportation mode in order to find out the optimum and demonstrated configuration of hybrid system. The current study is carried out in order to minimize the use of energy from fossil fuels and produce cleaner seas environment. The varying voyage speed are: depature from por/Arrival at Port 3 knots, Outward bound/Homeward bound 9.8 knots and on fishing ground 7 knots. The result of combining propulsion systems at sailing speed 3 knots with the optimum configuration was found in combination no 8 (Engine + Panel + Solar sail) and give emission index of 0,016, at fishing speed 7 knots and produces emission index of 0.05 and finally, at sailing speed 9.8 knots give emission index of 0.14

Keywords: HCFV; hybrid technology; power estimation; engine, solarpanel, sail, emission

## **1.Introduction**

A fishing vessel is a boat or ship used to catch fish in the sea, or on a lake or river [2]. According to the FAO, there are currently four million commercial fishing vessels. About 1.3 million of these are decked vessels with enclosed areas. Nearly all of these decked vessels are mechanized, and 40,000 of them are over 100 tons. At the other extreme, twothirds (1.8 million) of the undecked boats are traditional craft of various types, powered only by sail and oars [2]. Their catch provides daily foods for millions of people worldwide. It is recently reported that there is an increase on toxic gases such as  $CO_2$ ,  $SO_2$  and  $NO_X$  to the atmosphere, particularly with the use of diesel engine together with its fossil fuels. Given the impact of fishing, it is an important activity to enhance and align fishing operations with environmentally friendly practices [3]. Factors driving fishing vessel operational, in general, are economic and environmental issues. The main economic concern, in particular, is fuel costs and the main environmental issue amounts to emissions and pollution [4].

Normally voyage profile and sailing speed of fishing vessel in the world are: i) depature from por/Arrival at Port 3 knots, ii) Outward bound/Homeward bound 9.8 knots and iii)on fishing ground 7 knots [5].

Many efforts have been made to help the fishermen especially in order to reduce the use of fossil fuel. Several power systems have been developed including the combination of engine and sail which is later known as sail assisted engine [6]. The powering vessel without using engine and fuel oil later becomes more popular considering environmental issues known as green economy concept. There are several choices of power systems such as the use of sail, solar power and the combination of the two and three power systems [6]. The idea of developing HCFV appears from economic and environmental pressures thus combine to create the need for a fresh appraisal of the estimation of ship propulsive power and the choice of suitable machinery [4]. Economic factors such as changing fuel costs and environmental issues such as emission and pollution, all ultimately lead to the need to minimize ship propulsive power [4].

Figure 1 shows layout of the developed HCFV (with use power combination: engine, sail, photovoltaic). The large deck space is a key feature of catamaran fishing vessel, which provides an incredible amount of spaces for accommodation, bridge, engine room and massive fish storage. The current paper is attempted to develop the research from [3], with considering the environmental concern from the application of photovoltaic and sail in order to reduce the size of main engine for emission reduction purposes.



Figure 1: The Hybrid Catamaran Fishing Vessel

## 2. Power Estimation Methodology

The hybrid power of catamaran fishing vessel is designed to use an individual and combination of power by using conventional engine, PV panels and sail. It is firstly carried out by using the experiment result of catamaran resistance in towing tank [1], and followed by calculating the thrust requirement (T req.) and estimating the energy of power (P *req.*) of individual and later the combined power (diesel engine and sail, diesel engine and solar panels, sail and solar panels and diesel engine, sail and solar panels) in order to find out the optimum hybrid system at varying sailing speed. Furthermore, investigation is extended to the analysis of the reduction of  $CO_2$  Index, which used the formulation of fishing vessel approach proposed by [3].

#### 2.1 Data's set up

Given: the particular of catamaran and the result of experiment are shown in Tables 1 and 2, respectively, which is summarized from the work done in [1]:

Table 1: Particulars of catamaran

| Parameter    | Catamaran | Demihull |  |  |  |  |  |  |  |  |
|--------------|-----------|----------|--|--|--|--|--|--|--|--|
| LWL (m)      | 14.5      | 14.5     |  |  |  |  |  |  |  |  |
| B (m)        | 7.118     | 1.318    |  |  |  |  |  |  |  |  |
| H (m)        | 1.44      | 1.44     |  |  |  |  |  |  |  |  |
| D (m)        | 0.694     | 0.694    |  |  |  |  |  |  |  |  |
| CB           | 0.432     | 0.432    |  |  |  |  |  |  |  |  |
| Displ. (ton) | 11.8      | 5.9      |  |  |  |  |  |  |  |  |

 Table 2: Experiment result of catamaran resistance

| Run | V       | E.    | Catamaran Resistances (kN) |         |         |  |  |  |  |  |  |  |
|-----|---------|-------|----------------------------|---------|---------|--|--|--|--|--|--|--|
| No. | (knots) | Гſ    | S/L=0.2                    | S/L=0.3 | S/L=0.4 |  |  |  |  |  |  |  |
| 1   | 5.788   | 0.250 | 1.821                      | 1.659   | 1.659   |  |  |  |  |  |  |  |
| 2   | 6.218   | 0.268 | 2.141                      | 1.851   | 2.061   |  |  |  |  |  |  |  |
| 3   | 6.677   | 0.288 | 2.443                      | 2.239   | 2.348   |  |  |  |  |  |  |  |
| 4   | 7.051   | 0.304 | 2.852                      | 2.678   | 2.947   |  |  |  |  |  |  |  |
| 5   | 7.560   | 0.326 | 3.460                      | 3.568   | 3.547   |  |  |  |  |  |  |  |
| 6   | 8.032   | 0.347 | 4.467                      | 3.954   | 3.766   |  |  |  |  |  |  |  |
| 7   | 8.384   | 0.362 | 4.844                      | 4.345   | 4.341   |  |  |  |  |  |  |  |
| 8   | 8.818   | 0.380 | 5.149                      | 4.790   | 4.662   |  |  |  |  |  |  |  |
| 9   | 9.233   | 0.398 | 5.807                      | 5.592   | 5.515   |  |  |  |  |  |  |  |
| 10  | 9.813   | 0.423 | 7.101                      | 6.448   | 6.138   |  |  |  |  |  |  |  |

#### 2.2 Decision variables

#### 2.2.1 Ship Moving Theory

The overall concept of the powering system may be seen as converting the energy of the fuel into useful thrust (T req.) to match the ship resistance (RT) at the required speed (Vs) as shown in Figure 2.



Figure 2: Concepts of energy conversion

Based on the above concept, the requirement of ship moving is

$$T \ge R_T \quad or \quad T - R_T \ge 0 \tag{1}$$

To propel itself, the HCFV applies a combination various propulsors, which convert the power (engine electric) into useful thrust throughout: propeller and sail.

$$T req. = T propeller + T sail$$
 (2)

Where:

*T propeller* is thrust of propeller, *T sail* is thrust of sail

Hence

 $T \text{ propeller} + T \text{ sail} \ge R_T$ (3) This is later developed to power small vessels under a

This is later developed to power small vessels under a combined power known as hybrid system.

#### 2.2.2 Catamaran Resistance

The most widely used estimation of catamaran resistance is the method proposed by Insel and Molland [8]. In this case, catamaran hull consists of 2 isolated demihulls and creates wave and viscous resistance interference and formulated as follows:

$$C_T = (1 + \phi k)\sigma C_F + \tau C_W \tag{4}$$

Where:

 $C_T$  is total resistance coefficient,  $C_F$  is frictional resistance coefficient and obtained from ITTC-1957 correlation line,  $C_W$  is wave resistance coefficient of isolated demihull, (1+k) is form factor value of isolated demihull,  $\emptyset$  is used to estimate the change of pressure around demihull,  $\sigma$ represents additional velocity between demihulls and calculated from the summation of local frictional resistance around wetted surface area. In fact, the factors of  $\emptyset$  and  $\sigma$  are difficult to measure hence for the practical purposes, the two factors can be combined to form viscous resistance

interference factor  $\beta$  where  $(1 + \phi k)\sigma = (1 + \beta k)$  hence:

$$C_T = (1 + \beta k)C_F + \tau C_W$$
(5)

Where for monohull or demihull at isolation the value of  $\beta=1$  and  $\tau=1$ .

Hull resistance, 
$$R_H = \frac{1}{2} \cdot \rho \cdot C_T \cdot S \cdot V^2$$
 (5)

Air drag, 
$$D_{air} = C_D \cdot \frac{1}{2} \cdot \rho \cdot A_T \cdot V^2$$
 (6)

Total resistance,  $R_T = R_H + D_{air}$  (7)

#### 2.2.3 Thrust

Thrust is energy or force that required to propel the ship and can be expressed as the following equation [7]:

$$T req. = R_T / (1-t) \tag{8}$$

Where *t* is thrust deduction factor and (for single screw) may be calculated as [7]:

$$t = k_R \cdot wt \tag{9}$$

$$w_T = -0.0458 + 0.3745C_B^2 + 0.1590D_w - 0.8635Fr + 1.4773Fr^2$$
$$D_w = \frac{B}{p^{2}r^3} \sqrt{\frac{p^2r^3}{D}}$$

Where:  $k_R$  is 0.5 for thin rudder,  $w_T$  is wake fraction,  $C_B$  is block cefficient, Fr is Froude number, Dw is wake fraction parameter,  $\nabla$  is vessel displacement, B is breadth, D is depth.

#### 2.2.4 Powering

There are several types of propulsion, which can be used to assess the efficiency of propulsion and may be described as follows:

## 2.2.4.1 Conventional Engine

One fundamental division in conventional powering methods is the distinguish between the *effective power* required to drive the vessel and *power delivered* to the propulsion unit(s) [7].

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Effective power  $(PE) = R_T x V_s$  (10)

Delivered power 
$$(PD) = PE/\eta D$$
 (11)

Quasi propulsive coefficient  $(\eta D) = \eta P. \eta H. \eta R$  (12) where: Open water efficiency  $(\eta P)$ , Hull efficiency  $(\eta H) = (1-t)/(1-w_T)$ , Relative rotative efficiency  $(\eta R)$ 

Service power 
$$(Ps) = PD / \eta T$$
 (13)

Installed power (PI) = Ps + Margin (14) Margins (roughness, fouling, weather) 15 – 20% depend on service and route.

#### 2.2.4.2 Photovoltaic Panels

1

When a PV system is installed in a vessel, some obstacles must be overcome to extract the most power from the PV panels. A photovoltaic panel harvests most energy out of sun and then stores into battery. The energy is then used to power (electric engine) to propel the vessels into certain distance at certain speed [9]. The vessel is powered by battery and the PV power is applied to charge the battery during operational at sea. In this case, PV panels are placed on roof and sail as a solar sail. The solar sail has double function, namely producing the driving force in the direction of the motion and capturing energy from sun-rays.

Power requirement: 
$$P = V \times I$$
 (15)

$$Pmax = Voc x Isc x FF$$
(16)

Fill Factor: 
$$FF= \frac{Vmp \times Imp}{Voc \times Isc}$$
 (17)

P watt 
$$peak = PV$$
 area x PSI x  $\eta pv$  (18)

Where: Pmax : Power maximum (W), Voc: Open circuit voltage (V), Isc: Short circuit current (A), FF: Fill Factor, PV area : Photovoltaic area (m<sup>2</sup>), PS: *Peak Solar Insolation* 1000 W/m<sup>2</sup>,  $\eta pv$ : efficiency Photovoltaic

#### 2.2.4.3 Sail

A sail is defined as a surface, typically made of fabric and supported by a mast with purpose to propel a sailing vessel [11]. In estimating the performance of a sailing vessel, it is necessary to predict the forces generated by the sails [13].

Driving force 
$$(Ts) = q \cdot As$$
 (19)

Where : Dynamic wind pressure  $(q) = \frac{1}{2} \ge p \ge 1$   $x \ge p \ge 1$   $x \ge v_w^{2}$   $(ton/m^2)$ , Air mass density  $(p) = \frac{\gamma}{g}$ , Weight per unit volume  $(\gamma)=1.2265 \text{ t/m}^3$ ,  $g = \text{Acceleration of gravitation (} 9.81 \text{ ms}^{-2})$ ,  $\pounds = \text{Wind pressure Coeff. (} 1.1\text{)}$ , Wind speed  $(v_w)$ , Sail area (As).Practically, all boats have a sail ratio (SR) which sail area (As)/wetted surface (WSA) between 2.0 and 2.5, the mean value is 2.25 [11]. Using the graph of sail ratio shown in Figure 3, sail ratio depends on LWL of the vessel [12]. The choice of sail arrangement and underwater hull and appendage design can make a large difference in available speed for given wind directions and magnitudes [13]. However, in reality this depends not only on the apparent

wind speed and direction and the sail characteristics, but also on the skill of sailor in trimming the sails for the prevailing conditions [7].



#### 2.2.4.4 The combination of power

There are several power combination, which will be used in the HCFV, including diesel engine and sail; diesel engine and PV panels; sail, PV panels and diesel engine; solar sail, PV panels and diesel engine [6].

#### 2.2.5 Quantifying Environmental Impact

The emissions from ships include  $NO_X$ ,  $SO_X$  and  $CO_2$ .  $CO_2$  emissions have a global climate impact and a concentrated effort is being made worldwide towards their reduction. In order to monitor and quantify CO2 emissions, research from [3] explored about an estimation of greenhouse gasses per kg for fishing vessel. The general form of the Emission Index (*EI*) for fishing vessel, as proposed:

$$EI = Ki.SFR.KwT.\gamma$$
 (kg/day of CO<sub>2</sub>) (20)

For example: Ki 3170 Kg/Ton fuel, SFR 0.19 Kg/ Kw.hr, ship power (kW) 60 kW, T 8 hrs,  $\gamma$  0.03206 tons/kg (Diesel Oil type). By using Equation (20), it can be found that the Emission Index for fishing vessel (*EI*) 9,268 kg/day of CO<sub>2</sub>. It means that the HCFV using 60 kW diesel engine as converting the energy of the fossil fuels into useful thrust (*T*) to match the ship resistance (RT) at the required speed (*Vs*) and produce 9,268 kg/day of CO<sub>2</sub> pollutant. The current results give an estimate on the basis of ton of fuel burned times the factor *Ki* for exhaust gas and reflect the present fishing vessel operations where a fishing boat is assumed to be operated 8 hours per day.

#### **3. Results**

#### 3.1 Output Parameters

The results of total resistance  $(R_T)$  produced by (7), thrust requirement (*T req.*) calculated by (8), (9) and power requirement (*P req.*) estimated by (14) as shows in Table 3.

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|     |             |           |         |           |       |         |        | 1     |          | 0      |        |        |       |
|-----|-------------|-----------|---------|-----------|-------|---------|--------|-------|----------|--------|--------|--------|-------|
| No  | Source Va d | Va (Inta) | RT (kN) | Treq (kN) | Thrus | t suppl | y (kN) | Power | • supply | v (kW) | EI (K  | g/day) |       |
| 100 | power       | VS (KIS)  |         |           | E     | Р       | S      | Е     | Р        | S      | $CO_2$ | Index  |       |
| 1   | Engine (E)  |           |         | 0.115     |       | 0.115   | 0      | 0     | 7,04     | 0      | 0      | 1088   | 0,117 |
| 2   | Panel (P)   |           |         |           |       | 0       | 0.115  | 0     | 0        | 7,04   | 0      | 0      | 0     |
| 3   | Sail (S)    |           |         |           | 0     | 0       | 0.115  | 0     | 0        | 7,04   | 0      | 0      |       |
| 4   | E+ P        | 2         | 0.11    |           | 0.095 | 0.02    | 0      | 5,82  | 1,22     | 0      | 899    | 0,097  |       |
| 5   | E+ S        | 3         | 0.11    |           | 0.046 | 0       | 0.069  | 2,83  | 0        | 4,21   | 437    | 0,047  |       |
| 6   | P+S         |           |         |           | 0     | 0.02    | 0.095  | 0     | 1,22     | 5,82   | 0      | 0      |       |
| 7   | E+P+S       |           |         |           | 0.049 | 0.02    | 0.046  | 2,98  | 1,22     | 2,84   | 461    | 0,050  |       |
| 8   | E+P+SS      |           |         |           | 0.017 | 0.052   | 0.046  | 0,98  | 3,22     | 2,84   | 151    | 0,016  |       |

#### Table 3: Result of decision variables data's processing

## 3.2 Mathematic model

Total resistance, RT = 35.99 Fr2 + 1.633 Fr - 0.698Thrust requirement, Treq. = 37.85 Fr2 + 1.717 Fr - 0.736Power requirement, P req = 852.2 Fr2 - 289.9 Fr + 30.26

# **3.2.1** Mathematic model of Energy supply of *HCFV* on depature from port/Arrival Port at sailing speed 3 knots

Thrust requirement (T req.)



Figure 4: Correlation between Tp and Ts at Vs 3 knots





Figure 5: Correlation between Pp and Ps at Vs 3 knots

## Table 4: Energy supply of Power Combination at Vs 3 knots

| Run<br>No. | Vs (kts) | Fr    | <i>R<sub>H</sub>,</i><br>S/L0.4,<br>(kN) | D <sub>air</sub><br>(kN) | RT<br>(kN) | T req.<br>(kN) | P req.<br>(kW) |
|------------|----------|-------|--|--------------------------|------------|----------------|----------------|
| 1          | 5.788    | 0.25  | 1.659                                    | 0.294                    | 1.953      | 2.059          | 11.05          |
| 2          | 6.218    | 0.268 | 2.061                                    | 0.294                    | 2.355      | 2.443          | 13.78          |
| 3          | 6.677    | 0.288 | 2.348                                    | 0.294                    | 2.642      | 2.898          | 17.45          |
| 4          | 7.051    | 0.304 | 2.947                                    | 0.294                    | 3.241      | 3.284          | 20.89          |
| 5          | 7.56     | 0.326 | 3.547                                    | 0.294                    | 3.841      | 3.846          | 26.32          |
| 6          | 8.032    | 0.347 | 3.766                                    | 0.294                    | 4.06       | 4.417          | 32.28          |
| 7          | 8.384    | 0.362 | 4.341                                    | 0.294                    | 4.635      | 4.846          | 36.99          |
| 8          | 8.818    | 0.38  | 4.662                                    | 0.294                    | 4.956      | 5.382          | 43.16          |
| 9          | 9.233    | 0.398 | 5.515                                    | 0.294                    | 5.809      | 5.943          | 49.87          |
| 10         | 9.813    | 0.423 | 6.138                                    | 0.294                    | 6.432      | 6.763          | 60.12          |









Power requirement (P req.)



Figure 7: Correlation between Pp and Ps at Vs 7 knots

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| Table 5. Energy supply of I ower Combination at 7.5.7 knots |              |           |                    |            |                |                      |       |       |       |          |                 |       |      |   |
|---|--------------|-----------|--------------------|------------|----------------|----------------------|-------|-------|-------|----------|-----------------|-------|------|---|
| No  | <b>C</b>     | Va (Inta) | $DT (d_r M)$       | True (-NI) | $T_{reg}(d_N)$ | Thrust supply $(kN)$ |       |       | Powe  | r supply | EI (Kg/day)     |       |      |   |
| 110   | source power | VS (KIS)  | $\mathbf{M}$ (KIV) | Trey (KIV) | Е              | Р                    | S     | Е     | Р     | S        | CO <sub>2</sub> | Index |      |   |
| 1   | Engine (E)   |           |                    | 3,358      | 3,358          | 0                    | 0     | 21,77 | 0     | 0        | 3363            | 0,36  |      |   |
| 2   | Panel (P)    |           | 3,241              |            | 2 250          | 0                    | 3,358 | 0     | 0     | 21,77    | 0               | 0     | 0    |   |
| 3   | Sail (S)     |           |                    |            |                |                      | 0     | 0     | 3,358 | 0        | 0               | 21,77 | 0    | 0 |
| 4   | E+ P         | 7         |                    |            |                | 2,775                | 0,583 | 1,205 | 17,99 | 3,78     | 0               | 2779  | 0,30 |   |
| 5   | E+ S         | /         |                    |            | 1,352          | 0                    | 1,536 | 8,77  | 0     | 13,00    | 1354            | 0,15  |      |   |
| 6   | P+S          |           |                    |            | 0              | 0,583                | 1,352 | 0     | 3,78  | 17,99    | 0               | 0,00  |      |   |
| 7   | E+P+S        |           |                    |            | 1,423          | 0,583                | 1,205 | 9,23  | 3,78  | 8,76     | 1425            | 0,15  |      |   |
| 8   | E+P+SS       |           |                    |            | 0,470          | 1,536                | 1,536 | 3,06  | 9,95  | 8,76     | 472             | 0,05  |      |   |

Table 5. Energy supply of Power Combination at Vg 7 knots

3.2.2 Mathematic model of Energy supply of HCFV on outward bound/homeward bound at service speed 9.8 knots









Figure 9: Correlation between Pp and Ps at Vs 9.8 knots

| _ |     | Τε           | able 6: I | Energy s          | upply of P   | ower ( | Combi   | nation         | at Vs 9 | ).8 kno | ts |
|---|-----|--------------|-----------|-------------------|--------------|--------|---------|----------------|---------|---------|----|
|   | No  | Source power | Va (Inta) | DT (-N)           | I) True (AN) | Thrus  | t suppl | Power supply ( |         |         |    |
|   | 100 | Source power | VS (KIS)  | $\mathbf{M}$ (KN) | Treq (KN)    | Е      | Р       | S              | Е       | Р       |    |

| Ma  | Course mouse              | Va (Ista) | RT (kN) | DT (IN)    | Tung (IN) | $T(d_{\rm N})$ Tread $(d_{\rm N})$ |       | t suppl | V (KIN) | Power | r suppiy               | V (KW) | EI (K | g/aay) |  |  |       |       |       |       |       |       |      |
|-----|---------------------------|-----------|---------|------------|-----------|------------------------------------|-------|---------|---------|-------|------------------------|--------|-------|--------|--|--|-------|-------|-------|-------|-------|-------|------|
| 100 | source power              | VS (KIS)  |         | Ireq (KIN) | Е         | Р                                  | S     | Е       | Р       | S     | <b>CO</b> <sub>2</sub> | Index  |       |        |  |  |       |       |       |       |       |       |      |
| 1   | Engine (E)                |           |         |            | 6,689     | 0                                  | 0     | 60      | 0       | 0     | 9268                   | 1      |       |        |  |  |       |       |       |       |       |       |      |
| 2   | Panel (P)                 |           |         |            | 6,689     | 0                                  | 6,689 | 0       | 0       | 60    | 0                      | 0      | 0     |        |  |  |       |       |       |       |       |       |      |
| 3   | Sail (S)                  |           |         | 6,689      |           |                                    | 0     | 0       | 6,689   | 0     | 0                      | 0      | 0     | 0      |  |  |       |       |       |       |       |       |      |
| 4   | $\mathbf{E} + \mathbf{P}$ | 0.0       | 6 12    |            |           | 5,527                              | 1,162 | 2,399   | 49.58   | 10.42 | 0                      | 7659   | 0.83  |        |  |  |       |       |       |       |       |       |      |
| 5   | E + S                     | 9.8       | 0.45    |            |           | 2,693                              | 0     | 3,060   | 24.16   | 0     | 35.84                  | 3732   | 0.4   |        |  |  |       |       |       |       |       |       |      |
| 6   | P + S                     |           |         |            | 0         | 1,162                              | 2,693 | 0       | 10.42   | 49.58 | 0                      | 0      |       |        |  |  |       |       |       |       |       |       |      |
| 7   | E + P + S                 |           |         |            |           |                                    |       |         |         |       |                        |        |       |        |  |  | 2,834 | 1,162 | 2,399 | 25.43 | 10.42 | 24.15 | 3929 |
| 8   | E + P + Solar S           |           |         |            | 0,937     | 3,059                              | 3,060 | 8.42    | 27.43   | 24.15 | 1301                   | 0.14   |       |        |  |  |       |       |       |       |       |       |      |

## 4. Discussion

The first discussion is how the HCFV demonstrate the potential for using renewable energy on voyage:

- 1) Departure from port: the vessel in light weight condition at sailing speed 3 knots. Here, the vessel needed thrust (T req.) around 0.115 kN to equalize the ship resistance (RT) 0.112 kN and required power (P req.) is 7.04 kW. To fulfill Preq., the HCFV possible using powered, as follows: in bad condition, the vessel powered by engine (7.04 kW), it produces emission index (EI) of 1,088 kg/day of CO<sub>2</sub>. In good condition, possible uses all configuration as shown in Table 4. The optimum powered could be achieved when the vessel used combination no 8 (engine, panels and solar sail) because the EI is 0,016.
- 2) Outward bound: the vessel still in light weight condition at sailing speed Vs 9.8 knots. Here T req. is 6,689 kN, RT

is 6.432 kN and *P req.* is 60 kW. In operational, the vessel used engine, panels and solar sail together or substitute depending on weather condition. When the propel by engine, the EI is 9268 kg/day of CO<sub>2</sub>. The optimum powered find out in combination no 8 (engine, panels and solar sail), the EI is 0.14.

- 3) On fishing ground: Vs 7 knots used renewable wind and solar some times substitute or together depending on situation. At the lower fishing speed (7 knots) the engine could be switched off and the fishing vessel powered by the a combination of sail and solar panels. The power without pollution and no disturb the fishes. The result of Power Combination shows in Table 5.
- 4) Homeward bound: the vessel in cargo weight condition at sailing speed Vs 9.8 knots. The HCFV possible using powered, as follows: in bad condition, used engine (60 kW) and it produces emission index (EI) of 9,268 kg/day of CO2. In good condition, all of the configuration

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possible to used as shown in Table 6. But, the optimum powered could be achieved when the vessel using combination no 8 (engine, panels and solar sail) because the EI is 0.14

5) *Arrival at Port*: Vs 3 knots, used renewable solar panels some times substitute or together depending on situation.

The second discussion is how to applied the hybrid system could works in a combine power (engine, sail, PV) to propel the vessel. In this case, a combination various propulsors, which convert power available into useful thrust throughout: propeller and sail. To run the propeller, supplies power coming from engine and electric motor. Conventional engine needs converting the energy of the fuel into useful thrust (T) and leaning produce emission. PV panels were used to absorb energy from sun-rays and then saved it into battery, then battery supplies power to run electric motor and no pollution. The main propulsion as well as sail with purpose to propel a sailing vessel.

Figure 4 shows correlation between Tp and Ts at Vs 3 knots with mathematic function is Tp + Ts = 0.115

Figure 5. Correlation between Pp and Ps at Vs 7 knots with mathematic function is Pp + Ps = 7.04

Figure 6 shows correlation between Tp and Ts at Vs 7 knots with mathematic function is Tp + Ts = 3.235

Figure 7. Correlation between Pp and Ps at Vs 7 knots with mathematic function is Pp + Ps = 20.43

Figure 8 shows correlation between Tp and Ts at Vs 9.8 knots with mathematic function is Tp + Ts = 6,689.

To find out value Tp and Ts at Vs 9.8 knots is throughout the simple way. For example: when Ts = 0 Tp = 6.763, when Ts = 0.25Treq mean Tp=0.75 Treq. and so on. This is the explanation of equilibrium Tp and Ts works in hybrid system

Figure 9. Correlation between Pp and Ps at Vs 9.8 knots with mathematic function is Pp + Ps = 60. When the vessel uses individual power by engine (1), PV panels (2), sail (3) each produces thrust (T) is 6,689 kN or its similar with power 60 kW, as a power used to propel the vessel at the service speed ( $V_s$ ) 9.8 knots

In order to reduce the index of energy, a decrease in propulsive power must be achieved and/or improvements made in engine efficiency with a reduction in sfc. Improvements in efficiency of propulsion will lead directly to improvements in the economic return and a decrease in greenhouse gas effect (GHG) emissions. This means that there is now a double incentive to pursue such efficiency improvements. The ones of potential savings in resistance can be achieved throughout hull form selection. There are, however, some possible technical changes that will decrease emissions, but which may not be economically viable.

## 5. Conclusion

Based on the above discussion, it is discovered that the optimum hybrid system of fishing vessel combination was found in the result of combining propulsion systems at sailing speed 3 knots shown in Table 4 with the optimum configuration was found in combination no 8 (Engine + Panel + Solar sail) and give emission index of 0,016, at sailing speed 9.8 knots shown in Table 5 give emission index of 0.14 and finally, at fishing speed 7 knots shown in Table 6 produces emission index of 0.05. and it produces the lowest emission index. Therefore, current study is found to be very useful in order to minimize the use of energy from fossil fuels and produces cleaner seas environment.

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