Optimal Configuration of Converter for HVDC Transmission System

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Abstract: A novel method is proposed for configuring a power electronics converter circuit for optimal performance in HVDC transmission system. It is configured depending upon the desired output voltage pulses. Assuming high number of pulses in output voltage optimal configuration is obtained by achieving maximum possible output voltage, minimum Peak Inverse Voltage, and by obtaining transformer utilization factor value near unity. This paper suggests an analytical way of designing the converter circuit based on certain assumptions. A mathematical model of the scheme is developed. Detailed analysis and simulation results are presented in LabVIEW 7.1 software.

Keywords: HVDC, LabVIEW, power electronics Converter, PIV, TUF

1. Introduction

The driving force for the development of power systems is the on-going increase of electrical power demand. High Voltage Direct Current (HVDC) system plays vital role in today’s power system around the world and will continue to contribute more with the advent of Smart Super Grid in the future. Over the past few decades expanding power grids has proven to be both economically and environmentally desirable [1]. Presently power system operates under a high stress level which was neglected at the moment they were designed. The operating conditions of power system are being threatened form the reliability, controllability and security point of view. HVDC transmission brings a solution to have secure and improve the stability margins of power system [4]. The characteristic like having more flexibility and efficient power flow mechanism, as it provides a bidirectional power flow and is capable of controlling both active power and reactive power independently, to keep stable voltage and frequency [2]. It can prevent voltage collapse by using gradual P&Q modulation including reducing the active power to increase reactive power capability is needed. [16].

HVDC transmission resides a two basic type of converter technology. Those are classical line commutated current source converter (CSCs) where DC side polarity remain same, power flow decided by DC side voltage polarity and self-commutated voltage sourced converters (VSCs) where DC side voltage polarity will remain same, power flow direction decided by DC side current polarity [3]. Classical HVDC technology employs line commutated current source converters with thyristor valve used as a base technology for DC transmission. Where thyristors are not fully controlled switches, hence it put limitation to control mechanism used for controlled power flow [14]. Voltage source converter based transmission technology introduces flexibility in power transmission, as it uses fully controllable switches like IGBT which provides one of the efficient control mechanisms for control of power flow. Both classical and VSC-HVDC are used for the applications like long distance transmission, underground and undersea cable transmission and interconnection of asynchronous networks. [6]. Thyristor based classical HVDC mostly used for point to point large power transmission long distance over land or undersea cables [20]. It has certain disadvantage like commutation failure as thyristors can’t be off immediately, and it requires 40 ~ 60 % reactive power supply of the total active power transmission [17]. To have a solution IGBTs are used that can be switched off and on immediately, no commutation failure as thyristors can’t be off immediately, and it requires 40 ~ 60 % reactive power supply of the total active power transmission [17]. VSC -HVDC link consist of a back to back voltage sourced converters (VSCs), a common DC link, which includes a large DC capacitors and DC cables [18]. The control strategy is being designed to coordinate the active power control between two station which is realized by controlling the DC side voltage of one converter where other converter control the active power. Automatic control of power flow between stations is the result of a constant DC voltage source gives –slack bus”. [6]. AC voltage control and reactive power control will be switched as per the requirement. Power system operates closer to their stability limits, which may affect the damping of electromechanical oscillation and risks the system with a decreased system stability margin.

Configuration of an efficient and reliable HVDC converter is very important for the optimal operation of the HVDC transmission system [14]. It is experimentally proven that if the number of output pulses of the converter is high then the system gets much more proficient ripple free DC output and it will reduce the harmonics in AC side as well as the DC side. [9].But it is also not possible to have very large number of pulses, and then your circuit becomes very complex. In this paper HVDC converter has been configured for optimal performance of the system assuming 6 and 12 pulses. In the experimental result it is shown that specific configuration of converter circuit gives the optimal performance of the HVDC...
transmission system.

2. Characteristics of HVDC converter

For best possible performance in HVDC transmission system the converter must have the following characteristics:

2.1 High pulse number (p)

Large number of pulses will reduce the harmonics and hence filter circuit requirement will be less. So, the optimal number of pulse numbers normally the six pulse converters is very good, because the six pulses gives the desire the merits or features of converter circuit, six pulse is optimal. But at the same time, the two six pulses if shift by certain angle means 30 degree, twelve pulse can be obtained [13].

2.2 PIV/Vdo should be minimum

Peak inverse voltage (PIV) should be as low as possible if the peak inverse voltage is less here means less costly converter valve, means this is related directly to the cost of the converter [16]. Because the converter is consisting of your valves here; for large peak inverse voltage the cost of whole circuit is going to be more. So the ratio of PIV to converter output voltage (Vdo) should be minimum [8].

2.3 Vdo/R.M.S Voltage should be maximum

If any circuit which is giving more DC output voltage that is a better for same configuration. For the optimal converter design getting maximum possible output voltage is one of the major criteria [21].

2.4 Transformer Utilization Factor (TUF) should be close to unity

If converter is not properly configured then transformers are not utilized to their full potential [13]. Utilization factor is the best in the bridge rectifier circuit. That is why it is used very properly and in these circuits, all almost all of the applications. [22].

3. Mathematical model

For designing the mathematical model of the converter circuit the following assumptions are made:

- Supply to the converter is balanced 3phase supply
- All the semiconductor switches used in converter circuit are ideal switches
- Commutation overlap angle has been ignored

Leakage Reactance of the transformers are neglected
- Delay angle is assumed to be zero

Let,
- P is desired number of output voltage pulses of the converter
- q is number of valves in a commutating group
- r is number of parallel valves of converter circuit
- s is number of parallel valves of converter circuit
- Em is the Peak voltage

Output voltage of three pulse converter

\[ V_{do} = \frac{3}{2 \Pi} \int_{0}^{\frac{\Pi}{3}} Em\cos(\omega t) \, dt \]

so \[ V_{do} = \frac{3\sqrt{3}}{2 \Pi} \]

now this equation [1] can be generalized by-

\[ V_{do} = \frac{qsEm\sin(\frac{\Pi}{q})}{2 \Pi} \]

when \( q \) is even then

\[ PIV = \frac{2 \Pi}{qss\sin(\frac{\Pi}{q})} \]

When \( q \) is odd then

\[ PIV = \frac{\Pi}{qss\sin(\frac{\Pi}{2q})} \]

Transformer Utilization Factor can be expressed as

\[ TUF = \frac{\Pi}{\sqrt{2qss\sin(\frac{\Pi}{q})}} \]

Using the above mathematical equations with different combinations of \( q, r \) and \( s \) for a particular no of pulses optimal performing condition of a converter can be identified which is shown in result. [6].

4. Result and Discussions

Optimal configuration of converter is sized assuming the output voltage pulses of converter is 6 pulses.(i.e. \( p=6 \)) and 12 pulses (i.e. \( p=12 \)) is obtained by using the equation [2], [3], [4], [5].

<table>
<thead>
<tr>
<th>SL No</th>
<th>q</th>
<th>r</th>
<th>s</th>
<th>PIV/Vdo</th>
<th>Vdo/r.m.s voltage</th>
<th>TUF</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>2</td>
<td>1</td>
<td>3</td>
<td>1.0472</td>
<td>2.70092</td>
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<tr>
<td>3</td>
<td>3</td>
<td>1</td>
<td>2</td>
<td>1.2092</td>
<td>3.11876</td>
<td>1.48098</td>
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<tr>
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<td>3</td>
<td>2</td>
<td>1</td>
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<td>1.55938</td>
<td>1.48098</td>
</tr>
<tr>
<td>5</td>
<td>6</td>
<td>1</td>
<td>1</td>
<td>2.0944</td>
<td>5.40185</td>
<td>1.81382</td>
</tr>
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</table>
A programming has been developed using the mathematical model for identification of optimal configuration HVDC converter in LabVIEW 7.1 software [29]. Table 1 shows the result for different combination of \( q, r \) and \( s \) when no of pulse \( p \) is taken as 6. It is observed that when the combination is \( q=3, r=1 \) and \( s=2 \) then the converter satisfies all the criteria for optimal performance. The highlighted row (3rd row) of Table 1 shows PIV/ \( V_{od} \) is less, \( V_{od} \)/r.m.s voltage also gives increased output voltage and TUF is also nearly unity with this combination. Figure 1 shows graphical display of programming output and detects optimal converter circuit configuration for best performance on HVDC transmission system.

**Table 2: Optimal performance of 12 pulse converter**

<table>
<thead>
<tr>
<th>SL No</th>
<th>( q )</th>
<th>( r )</th>
<th>( s )</th>
<th>PIV/ ( V_{od} )</th>
<th>( V_{od} )/r.m.s voltage</th>
<th>TUF</th>
</tr>
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<tr>
<td>1</td>
<td>12</td>
<td>1</td>
<td>1</td>
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<td>20.8711</td>
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<td>1.81382</td>
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<td>3</td>
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<td>2.0944</td>
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<td>1.81382</td>
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<td>2</td>
<td>1.2092</td>
<td>3.11876</td>
<td>1.48098</td>
</tr>
</tbody>
</table>

Figure 1: Front panel view of LabVIEW program for Identification of optimal 6 pulse converter configuration (a)variation of PIV, \( V_{od} \), TUF with different combination of \( q, r, s \) with time, (b) PIV voltage variation, (c) Converter output voltage variation, (d) TUF variation.
The programming has been also tested on 12 pulse converter and results have been tabulated on Table 2; the highlighted row (5th row) of Table 2 shows optimal performance [33]. In the graph figure 2 shows when the combination of the converter circuit has the following values $q=3, r=1$ and $s=4$ then Peak Inverse Voltage ratings is lowered significantly so converter valves don’t have to block high PIV and converter cost will be less and in this configuration converter output voltage also increased and TUF is nearly unity which means transformer can also be utilized efficiently.

But if any other values of $q,r,s$ are taken converter do not give desired performance for example if $q=12,r=1,s=1$ then converter output is very high but PIV is also excessively high which increases the converter valve rating and thus cost of the converter increases. In this condition TUF is also well away from unity.

5. Conclusions

This paper suggests the configuration of a cost effective reliable HVDC converters. This optimal configured converted not only improves the HVDC transmission system performance but it also improves the efficiency of transformers used at the AC supply end. As the HVDC system has become popular due to the requirement of power transmission over long distance so this optimal configuration technique of converter can be used for better performance. This converter can be used in multilink HVDC system, Hybrid AC/DC system, Micro grid systems, Wind power generating station.

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