## Influence of the Autoclaving Processes on the Most Commonly Used Orthodontic Archwires

# Valery Petrov, DMD, PhD<sup>1</sup>, Laura Andreeva, DMD, PhD<sup>2</sup>, Mirella Gueorguieva<sup>3</sup>, Stanimira Terzieva, PhD<sup>4</sup>, Angelina Stoyanova-Ivanova, PhD<sup>5</sup>, Valdek Mikli, PhD<sup>6</sup>

<sup>1, 2, 3</sup>Department of Orthodontics, Faculty of Dental Medicine, Medical University – Sofia, 1 St. Georgi Sofiiski Blvd., 1431 Sofia, Bulgaria

<sup>4, 5</sup>Georgi Nadjakov Institute of Solid State Physics, Bulgarian Academy of Sciences, 72 Tzarigradsko Chaussee Blvd., 1784 Sofia, Bulgaria

<sup>6</sup>Department of Materials Science, Tallinn University of Technology, Ehitajate 5, 19086 Tallinn, Estonia

Abstract: The orthodontic archwires are an integral part of the fixed appliance used for treatment of orthodontic malocclusions. The specific requirements for the prevention and control of care associated infections necessitates that every orthodontist should prevent contaminated orthodontic archwires being placed in the patient's mouth. Most leading companies offer their products in individual sealed packages suitable for autoclaving. The aim of this study is to determine the changes occurring in the chemical composition and the surface of four of the wires most widely used in the orthodontic practice. For comparison, the wires are divided into two groups: a control group and a group of wires sterilized in a type B autoclave at 121 °C for 21 min.

Keywords: autoclaving process, orthodontic archwires

## 1. Introduction

The specific requirements towards prevention and control of cross-contamination necessitates that the orthodontists should avoid placing contaminated orthodontic arches into the patient's mouth. Most leading companies offer their products in individual hermetically sealed packages suitable for autoclaving. Research on studying the possible changes in the orthodontic archwires during the autoclaving processes have been carried out since the late 1980s; basically, the studies have had to do with the mechanical properties assessed through tests of tensile strength and bending. The results obtained have been contradictory; some authors have concluded that the sterilization leads to a change of the mechanical properties, while others have observed no differences [1-6].

Pernier C. et al. [7] investigated the effect of the autoclaving on the surface parameters and on the mechanical properties of six orthodontic archwires. The archwires analyzed were of stainless steel, nickel-titanium and titanium-molybdenum. Their mechanical properties were evaluated by three point tests for bending. The results achieved indicated that the autoclaving did not have harmful effects on the surface parameters and on the corresponding mechanical properties.

It is known that any change in the chemical composition of a given alloy leads to changes in its properties. The aim of the present study was to monitor the influence of the autoclaving processes on the chemical composition and on the surface of four of the orthodontic archwires most widely used in practice. The orthodontic arches were made of the following types of alloys: chromium-nickel stainless steel, nickeltitanium, titanium-molybdenum and copper-nickel-titanium, with a size of 0.016  $\times$  0.022 inches. The archwires were divided into two groups: a control group and a group of autoclaved archwires. The autoclaving was carried out in a type B autoclave at 121 °C for a period of 21 min.

## 2. Materials and Experimental Methods

#### 2.1. Materials

For each of the orthodontic archwires investigated, three segments were selected (one frontal and two side ones), where the corresponding analyses were conducted. It is important to know whether the autoclaving can be carried out for all types of orthodontic arches, regardless of what alloy they are made, and to determine whether the process has any adverse effects on the archwires' surface structure. The study of the changes in the chemical composition and the surface characteristics of the as-received and of the as-received autoclaved orthodontic arches allows one to determine whether the autoclaving processes influences their properties. Table 1 shows the types of the archwires investigated.

Table 1: List of investigated orthodontic wires.

	U	
Type of	Cross section	Category of
orthodontic wires	[inches]	orthodontic wires
A – stainless steel	0.016 x 0.022	A0 – as -received
		A1 – sterilized
B – nickel-titanium	0.016 x 0.022	B0 - as -received
		B1 – sterilized
C – beta-titanium	0.016 x 0.022	C0 – as -received
		C1 - sterilized
D – copper-nickel-	0.016 x 0.022	D0 – as -received
titanium		D1 – sterilized

#### 2.2. Experimental Methods

The wires were analyzed by scanning electron microscopy (SEM) and X-ray energy dispersive spectroscopy (EDS). The microstructure of the wires surface was studied by means of a Zeiss EVO MA-15 scanning electron microscope with a LaB6 cathode on polished cross-section samples. The chemical composition was determined by EDS using an Oxford Instruments INCA Energy system. The qualitative and quantitative analyses were carried out at an accelerating voltage of 20 kV, an optimal condition for these samples.

## 3. Results and Discussion

Analyzing the composition of the archwires studied, we compared the data obtained about the new as-received archwires with the data in the scientific literature and found a good agreement. The EDS analysis of the elemental composition of the stainless steel archwires confirmed that made by [8, 9]. In the nickel-titanium (Ni-Ti) archwires, the percentage ratios of nickel and titanium were the same as those quoted by [9, 10]. For the thermally-activated (TMA) archwires, the analysis again confirmed the data of [11] for the chemical composition of the titanium-molybdenum alloy wires.

In Ni-Ti archwires, we observed an increase in the titanium content by + 0.17%, and a decrease of the nickel content by 0.17%, which we attribited to the experimental error (Table 3). The deviations are without a statistically significant difference, and are within the values cited in the literature [12, 13]. In the other types of arches – beta-titanium (C) and copper-nickel-titanium (D) - we observed insignificant changes in the chemical composition. In the stainless steel archwires (A), we found a significant increase in the iron content (+0.59%, Table 2), which is likely due to variations in the composition of the different batches of archwires, or to deposits on the archwires caused by water vapor in the autoclave after drying [14]. Table 2 shows the results for the chemical composition of a steel orthodontic archwire (A), unused and unused sterilized (autoclaved), as obtained by the EDS analysis. The data are compared with sources from the literature [9, 13].

**Table 2:** Elemental content of as-received and of sterilized type A wires.

Elements,	Si	Cr	Mn	Fe	Ni	Total
weight %						
Industrial data	~1	18÷20	~2	~ 71	8÷11	
(information)						
A0						
(as-received)						
Initial	0.82	19.76	1.54	69.08	8.80	100
components content						
A1						
Mean components						
content after	0.82	19.70	1.44	69.67	8.38	100
sterilization process						
	0	-0.06	-0.1	+0.59	-0.42	

The study of the chemical composition of the type A wires (as-received and as-received sterilized) demonstrated no

statistically significant difference. The changes seen in the amount of iron with a higher average value of 0.59%, and a lower average value of amount of nickel of 0.42%, should not be expected to affect the surface and the properties of the material. Figure 1 shows the microstructures of the surfaces of the unused and unused sterilized (A) archwires respectively, as studied by a scanning electron microscope.



Figure 1: Scanning electron images of the surface of SS steel archwires, A0 - as-received A1 - as-received sterilized (autoclaved).

The above measurements did not establish any changes on the surface structure of the archwires. Processes of corrosion or increased roughness were not observed. The practically negligible differences that we found were likely due to the fact that the studies were carried out at different points, the alloy not being completely homogeneous, or to the equipment's measurement error. We can note that the surface of the steel archwires was the smoothest compared to the other archwires tested. The data obtained by the EDS analysis about the ratio of the elements in the nickel-titanium orthodontic archwires before and after autoclaving are provided in Table 3, together with the data quoted in the references.

B wires			
Elements,	Ni	Ti	Total
weight %			
Industrial data (information)	54÷55 %	43÷44 %	
B0 (as-received) Initial components	54.56	45.44	100
Content			
B1 - Mean components content after	54.73	45.27	100
sterilization process			
	+0.17	-0.17	

 Table 3: Elemental content of as-received and sterilized type

 B wires

The data about the Ni-Ti archwires made it obvious that the changes in the chemical composition were 0.17 %, while there were no visible changes on the surface, whose images are shown in Figure 2.

#### International Journal of Science and Research (IJSR) ISSN (Online): 2319-7064 Index Copernicus Value (2013): 6.14 | Impact Factor (2013): 4.438



Figure 2: Scanning electron images of nickel-titanium archwires' surface of, B0 - as-received and B1 - as-received sterilized (autoclaved).

The SEM images showed surface irregularities. According to Pernier et al. [7] and Van Hoogstraten et al. [15], the higher degree of roughness can be explained by the fact that the sterilization removes residues and oily traces that may have remained in the archwires after their production. The results of the EDS analysis of as-received and as-received sterilized orthodontic archwires of beta-titanium alloy (C) established minor changes in the chemical composition, namely, +0.10% to -0.15%, which is within the existing method's error (Table 4). No signs of corrosion could be seen on surface (Figure 3).

**Table 4:** Elemental content of as-received and sterilized type

C wires.					
Elements, weight %	Ti	Zr	Mo	Sn	Total
Industrial data (information)	~79 %	~6 %	~11 %	~4 %	
C0 (as-received) Initial components content	76.80	6.74	11.75	4.71	100
C1 – Mean components content after sterilization process	76.84	6.59	11.75	4.81	100
	+0.04	-0.15	0	+0.10	

The thermally-activated archwires are characterized by structural transformations during changes in the temperature (martensite-austenite). Bearing this in mind, we performed X-ray structural analysis for these orthodontic archwires (Figure 4) on the as-received and as-received autoclaved archwires with copper content (D1). The analysis showed that after the sterilization processes there were no structural changes in the thermally-activated archwires.



Figure 3: Scanning electronic images of the surface of TMA archwire, C0 - as-received and C1 - as-received sterilized (autoclaved).



Figure 4: X-ray spectra of thermally-activateed archwires with copper content: as-received (black) and as-received (autoclaved) (red).

In these, as well as in the other orthodontic archwires studied, no significant changes on the surface were observed due to the autoclaving process (Figure 5). The differences established in the chemical composition were within the experimental error, while no corrosion processes were seen on the surface (Table 5).

Bearing in mind the above, we believe we can summarize the results by concluding that the autoclaving processes did not affect the crystal structure and the parameters of the archwires investigated. The analyses carried out by SEM and by EDS did not reveal statistically significant changes in the chemical composition of the autoclaved archwires. A possible reason for the variations observed in the chemical composition was the complexity of the production procedures on the one hand, and on the other, the difference in the properties of the archwires within separate batches. This finding strongly limits the consistency of the experimental data [7].



**Figure 5:** Scanning electronic images of the surface of thermally-activated orthodontic archwire with copper content, D0 - as-received D1 - as-received autoclaved.

	D wir	es			
Elements,	Ti	Ni	Си	Cr	Total
weight %					
Industrial data	~43 %	~50 %	~6.5 %	~0.5%	
(information)					
D0 (as-received)	45.58	48.39	5.56	0.47	100
Initial components					
content					
D1- Mean components	45.60	48.33	5.66	0.41	100
content after					
sterilization process					
	+0.02	-0.06	+0.10	-0.06	

Table 5: Elemental content of as-received and sterilize	d type
---	--------

## 4. Conclusions

The lack of statistically significant differences established in the study of new and autoclaved orthodontic archwires gives us reason to conclude that the orthodontic arches can be sterilized because the autoclaving processes do not affect their properties and the orthodontists could thus ensure the maximum safety of their patients.

## References

- J. E. Buckthal, M. J. Mayhew, R. P. Kusy, J. J. Crawford, "Survey of sterilization and disinfection properties", J Clin Orthod, 20, pp. 759-65,1986.
- [2] J. E. Buckthal, R. P. Kusy, "Effects of cold disinfectants of the mechanical properties and the surface topography of nickel titanium arch wires", Am J Orthod Dentofacial Orthop., 84, pp. 117-22, 1988.
- [3] M. J. Mayhew, R. P. Kusy, E"ffects of sterilization on the mechanical properties and the surface topography of nickel-titanium arch wires", Am J Orthod Dentofacial Orthop., 93, pp. 232-6 1988.
- [4] Kapila S, Haugen JW, Watanabe LG. Load-deflection characteristics of nickel-titanium alloy wires after

clinical recycling and dry heat sterilization. Am J Orthod Dentofacial Orthop 1992; 10: 120-6.

- [5] G. A. Smith, J. A. von Fraunhofer, G. R. Casey, "The effect of clinical use and sterilization on selected orthodontic arch wires", Am. J Orthod Dentofac Orthop., 102, pp. 153-159 1992.
- [6] J. A. Staggers, D. Margeson, "The effects of sterilization on the tensile strength of orthodontic wires", Angle Orthodontist 63, pp. 141 – 144, 1993.
- [7] C. Pernier, et al. "Influence of autoclave sterilization on the surface parameters and mechanical properties of six orthodontic wires", European Journal of Orthodontics, 27, pp. 72-81 2010.
- [8] R. S. de Biasi, A. C. O. Ruela, C. N. Elias, O. Chevitarese, "The influence of heat treatment in orthodontic arches made of stainless steel wires", Mater. Res., 3, pp. 97-8, 2000.
- [9] W. A. Brantley, Orthodontic wires. In: Brantley WA, Eliades T, eds. Orthodontic Materials: Scientific and Clinical Aspects. Stuttgart: Thieme, pp. 77-103, 2001.
- [10] W. J. Buehler, R. C. Wiley, "Ti-Ni Ductile intermetallic compound", Trans ASM, 55, pp. 269-276, 1962.
- [11] A. J. Goldberg, C. J. Burstone, "Status report on betatitanium orthodontic wires Council on Dental Materials, Instruments, and Equipment", J Am Dent Assoc., 105, pp. 684-5, 1982.
- [12] C. J. Burstone, A. J. Goldberg, "Beta titanium: a new orthodontic alloy", Am J Orthod., 77, pp. 121-32, 1980.
- [13] T. P. Chaturvedi, "Corrosion Behavior of Orthodontic Alloys", The Orthodontic Cyber Journal, January, 2008, [Online] Available: <u>www.orthocj.com</u>
- [14] J. C. Keller, R. A. Draughn, J. P. Wightman, W. J. Dougherty, S. D. Meletiou, "Characterization of sterilized CP titanium implant surfaces", International Journal of Maxillofacial Implants, 5, pp. 360-367, 1990.
- [15] I. M. Van Hoogstraten, K. E. Andersen, B. M. Von Blomberg, et al. "Reduced frequency of nickel allergy upon oral nickel contact at an early age", Clin Exp Immunol., 85, pp. 441–445, 1991.