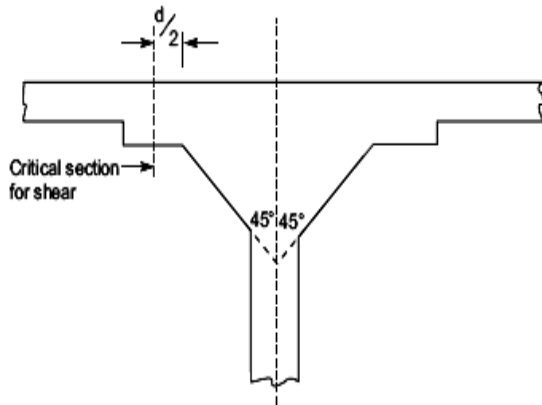


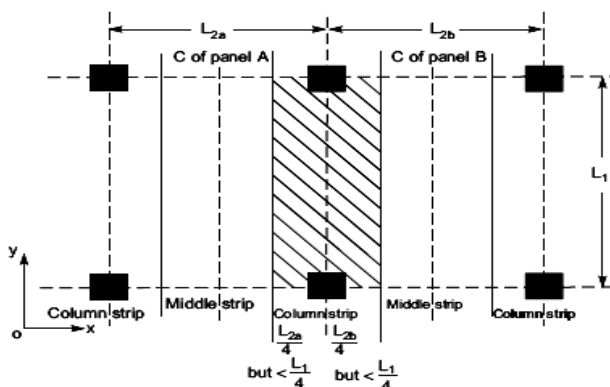
**Figure 3.3:** Slab with Drop and Column without Column Head

- (i) Slabs without drop and column head (Figure 3.1).
- (ii) Slabs without drop and column with column head (Figure 3.2).
- (iii) Slabs with drop and column without column head (Figure 3.3).
- (iv) Slabs with drop and column head as shown in (Figure 3.4)



**Figure 3.4:** Slab with Drop and Column with Column Head

The portion of flat slab that is bound on each of its four sides by centre lines of adjacent columns is called a panel. The panel shown in figure 3.5 has size  $L_1 \times L_2$ . A panel may be divided into column strips and middle strips. Column Strip means a design strip having a width of  $0.25L_1$  or  $0.25L_2$ , whichever is less. The remaining middle portion which is bound by the column strips is called middle strip. Figure 3.5 shows the division of flat slab panel into column and middle strips in the direction y.



**Figure 3.5:** Panel Column Strips and Middle Strip in Y-Direction

**Proportioning of Flat Slabs**

IS 456-2000 [Clause 31.2] gives the following guidelines for proportioning.

**3.2.1 Drops**

The drops when provided shall be rectangular in plan, and have a length in each direction not less than one third of the panel in that direction. For exterior panels, the width of drops at right angles to the non continuous edge and measured from the centre-line of the columns shall be equal to one half of the width of drop for interior panels.

**3.2.2 Column heads**

Where column heads are provided, that portion of the column head which lies within the largest right circular cone or pyramid entirely within the outlines of the column and the column head, shall be considered for design purpose as shown in figure 3.2 and 3.4

**3.2.3 Thickness of flat Slab**

The thickness of the flat slab up to spans of 10 m shall be generally controlled by considerations of span(  $L$  ) to effective depth (  $d$  ) ratios given as below:

**Table 1: Span to depth ratio**

Cantilever	7
Simply supported	20
Continuous	26

For slabs with drops, span to effective depth ratios given above shall be applied directly; otherwise the span to effective depth ratios in accordance with above shall be multiplied by 0.9. For this purpose, the longer span of the panel shall be considered. The minimum thickness of slab shall be 125 mm.

**3.3 Analysis and Design of Flat Slab for Vertical Load**

For this IS 456-2000 permits use of any one of the following two methods:

- The Direct Design Method
- The Equivalent Frame Method

**3.1 The direct design method**

This method has the limitation that it can be used only if the following conditions are fulfilled. There shall be minimum of three continuous spans in each direction. The panels shall be rectangular and the ratio of the longer span to the shorter span within a panel shall not be greater than 2. The successive span length in each direction shall not differ by more than one-third of longer span. The design live load shall not exceed three times the design dead load. The end span must be shorter but not greater than the interior span. It shall be permissible to offset columns a maximum of 10 percent of the span in the direction of the offset not with standing the provision in (b).

**Total Design Moment**

The absolute sum of the positive and negative moment in each direction is given by

$$M_0 = \frac{W L_n}{8}$$

Where,

$M_0$  = Total moment

$W$  = Design load on the area  $L_2 \times L_n$

$L_n$  = Clear span extending from face to face of columns, capitals, brackets

or walls but not less than  $0.65 L_1$

$L_1$  = Length of span in the direction of  $M_0$ ; and

$L_2$  = Length of span transverse to  $L_1$

In taking the values of  $L_n$ ,  $L_1$  and  $L_2$ , the following clauses are to be carefully noted

When the transverse span of the panel on either side of the centre line of support varies,

$L_2$  shall be taken as the average of the transverse spans. In

Fig. 1.5 it is given by  $\frac{(L_{2a} \times L_{2b})}{2}$ .

When the span adjacent and parallel to an edge is being considered, the distance from to the centre-line of the panel shall be substituted for  $L_2$ . Distribution of Bending Moment in to -ve and +ve Moments

The total design moment  $M_0$  in a panel is to be distributed into -ve moment and +ve moment as specified below.

In an interior span

Negative Design Moment  $0.65 M_0$

Positive Design Moment  $0.35 M_0$

In an end span

Interior negative design moment

$$= \left[ 0.75 - \frac{0.10}{1 + \frac{1}{\alpha_c}} \right] M_0$$

Positive design moment

$$= \left[ 0.63 - \frac{0.28}{1 + \frac{1}{\alpha_c}} \right] M_0$$

Exterior negative design moment

$$= \left[ \frac{0.65}{1 + \frac{1}{\alpha_c}} \right] M_0$$

where  $\alpha_c$  is the ratio of flexural stiffness at the exterior columns to the flexural stiffness of the slab at a joint taken in the direction moments are being determined and is given by

$$\alpha_c = \frac{\sum k_c}{\sum k_s}$$

Where,  $K_c$  = Sum of the flexural stiffness of the columns meeting at the joint; and

$K_s$  = Flexural stiffness of the slab, expressed as moment per unit rotation.

Distribution of Bending Moment across the Panel Width

The +ve and -ve moments found are to be distributed across the column strip in a panel as shown in table 3.1. The moment in the middle strip shall be the difference between panel and the column strip moments.

Table 3.1: Distribution of Moment across the Panel Width in a Column Strip

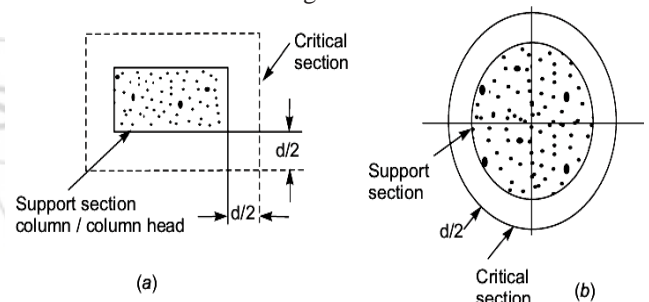
**Table 2: Percentage of Moment**

Sr. No.	Distributed Moment	Percent of Total Moment
A	Negative BM at the exterior support	100
B	Negative BM at the interior support	75
C	Positive bending moment	60

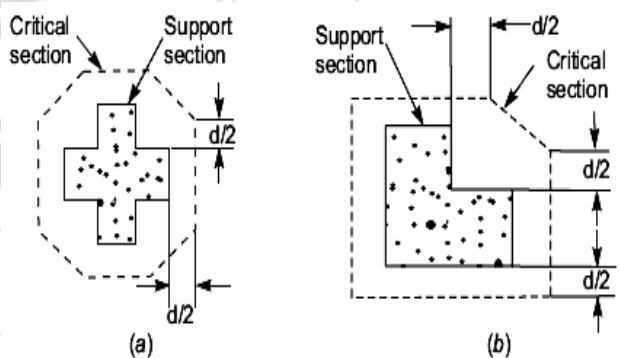
**Moment in Column**

In this type of constructions column moments are to be modified as suggested in IS 456-2000 [Clause No. 31.4.5]. shear Force

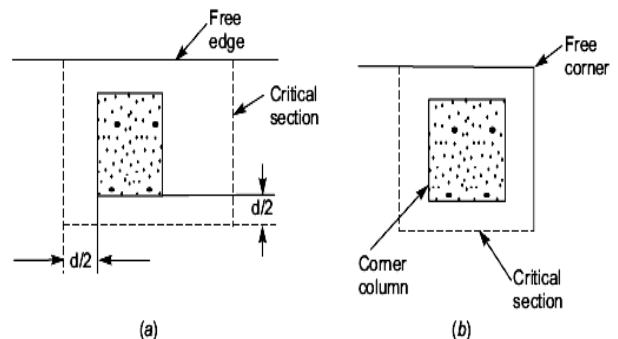
The critical section for shear shall be at a distance  $\frac{d}{2}$  from the periphery of the column/capital drop panel. Hence if drops are provided there are two critical sections near columns. These critical sections are shown in figure . The shape of the critical section in plan is similar to the support immediately below the slab as shown in figure



**Figure 3.6: Critical Section for Shear**



**Figure 3.7: Critical Section for Columns Sections with Re-Entrant Angles**



**Figure 3.8: Critical Section for Columns near the Free Edge of a Slab**

The nominal shear stress may be calculated as

$$\tau_v = \frac{V}{b_o d}$$

Where,  $V$  – is shear force due to design  
 $b_0$  – is the periphery of the critical section  
 $d$  – is the effective depth

The permissible shear stress in concrete may be calculated as  $k_s \tau_c$ ,

where  $k_s = 0.5 + \beta_c$  but not greater than 1, where  $\beta_c$  is the ratio of short side to long side of the column/capital; and

$$\tau_c = 0.25 \sqrt{f_{ck}}$$

If shear stress  $\tau_v < \tau_c$  - no shear reinforcement are required. If  $\tau_c < \tau_v < 1.5 \tau_c$ , shear reinforcement shall be provided. If shear stress exceeds  $1.5 \tau_c$  flat slab shall be redesigned.

### 3.3.2 Equivalent frame method

IS 456–2000 recommends the analysis of flat slab and column structure as a rigid frame to get design moment and shear forces with the following assumptions:

Beam portion of frame is taken as equivalent to the moment of inertia of flat slab bounded laterally by centre line of the panel on each side of the centre line of the column. In frames adjacent and parallel to an edge beam portion shall be equal to flat slab bounded by the edge and the centre line of the adjacent panel.

Moment of inertia of the members of the frame may be taken as that of the gross section of the concrete alone.

Variation of moment of inertia along the axis of the slab on account of provision of drops shall be taken into account. In the case of recessed or coffered slab which is made solid in the region of the columns, the stiffening effect may be ignored provided the solid part of the slab does not extend more than  $0.15 l_{ef}$  into the span measured from the centre line of the columns. The stiffening effect of flared columns heads may be ignored.

Analysis of frame may be carried out with substitute frame method or any other accepted method like moment distribution or matrix method.

### Loading Pattern

When the live load does not exceed  $\frac{3}{4}$ th of dead load, the maximum moments may be assumed to occur at all sections when full design live load is on the entire slab.

If live load exceeds  $\frac{3}{4}$ th dead load analysis is to be carried out for the following pattern of loading also:

(i) To get maximum moment near mid span –  $\frac{3}{4}$ th of live load on the panel and full live load on alternate panel

(ii) To get maximum moment in the slab near the support –  $\frac{3}{4}$ th of live load is on the adjacent panel only

It is to be carefully noted that in no case design moment shall be taken to be less than those occurring with full design live load on all panels. The moments determined in the beam of frame (flat slab) may be reduced in such proportion that the numerical sum of positive and average negative moments is not less than the value of total design moment  $M_0 = \frac{W L_n}{8}$ .

The distribution of slab moments into column strips and

middle strips is to be made in the same manner as specified in direct design method.

### 3.3.3 Slab reinforcement Spacing

The spacing of bars in a flat slab shall not exceed 2 times the slab thickness.

### Area of Reinforcement

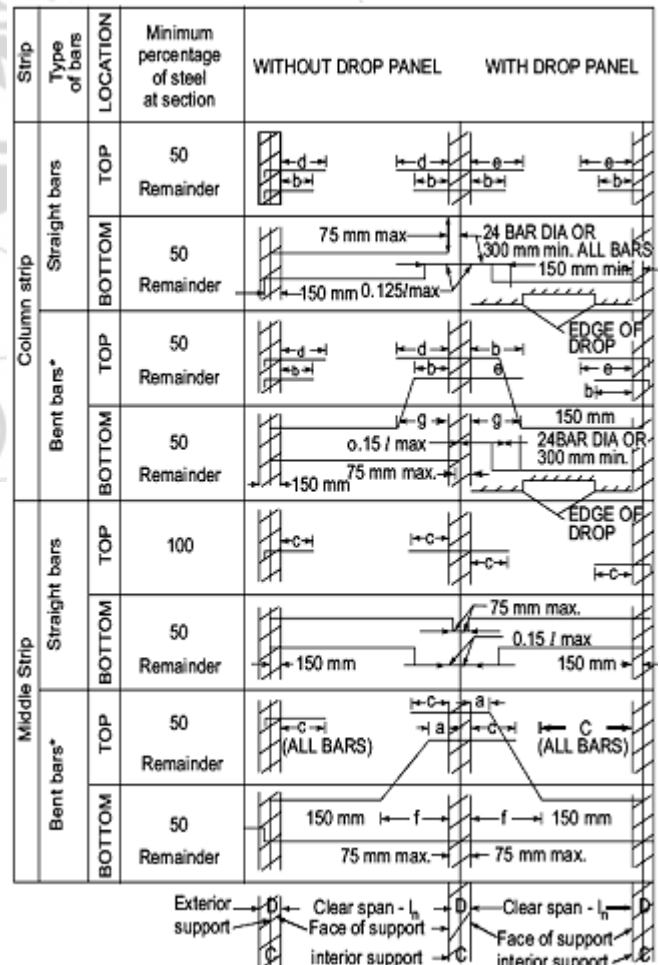
When the drop panels are used, the thickness of drop panel for determining area of reinforcement shall be the lesser of the following:

- Thickness of drop, and
- Thickness of slab plus one quarter the distance between edge of drop and edge of capital.

The minimum percentage of the reinforcement is same as that in solid slab i.e., 0.12 percent if HYSD bars used and 0.15 percent, if mild steel is used.

### Minimum Length of Reinforcement

At least 50 percent of bottom bars should be from support to support. The rest may be bent up. The minimum length of different reinforcement in flat slabs should be as shown in figure 1.9 (Figure 16 in IS 456–2000). If adjacent spans are not equal, the extension of the –ve reinforcement beyond each face shall be based on the longer span. All slab reinforcement should be anchored properly at discontinuous edges.



**Figure 3.9: Minimum Bend Joint and Extension for Reinforcement in Flat Slab (IS 456-2000)**

#### 4. Conclusion

This study present a complete detail procedure of analysis and design of flat slab structure with is 456:2000. in this paper follow the guideline given by the is code and limitation of it. flat slab gives the advantage over beam slab structure. this slab increase efficiency of structure and require less construction cost as compare to beam slab construction. this paper gives the guideline for selection of drop , panel width, slab thickness and gives the reinforcement details.

#### References

- [1] M. Altug Erberik, Amr S. Elnashai "Fragility analysis of flat-slab structures " University of Illinois at Urbana–Champaign, 205 Mathews Avenue, Urbana, IL 61801-2352, USA.
- [2] SumitPahwa ,Vivek Tiwari "Comparative Study of Flat Slab with Old Traditional Two Way Slab" International Journal of Latest Trends in Engineering and Technology Vol. 4 Issue 2 July 2014.
- [3] Sahana T.S "Use Of Flat Slabs In Multi-Storey Commercial Building Situated In High Seismic Zone" IJRET Volume: 03 Issue: 08 | Aug-2014
- [4] IS456:2000 plan and reinforced concrete code of practices

